# LAWRENCE FIELD OPERATIONS FACILITY <br> Combined Facility for the Municipal Services and Operations <br> Organization (MSO) <br> Northeast of E 19th Street \& O'Connell Road CFS Project Number 191196 

## Traffic Study

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## Introduction

This traffic study for the field operations campus in the City of Lawrence, Kansas, has been prepared at the request of the City of Lawrence in accordance with the City's Traffic Study Guidelines. The City of Lawrence is constructing a new field operations campus on the eastern side of the city which will consolidate several departments into one secure location. The 168 acre site will be northwest of the intersection of E 19th Street \& O’Connell Road. Proposed staff includes 223 full-time and 13 part-time personnel with some individuals making multiple site trips to and from the facility throughout the day. The facility will be constructed to accommodate a growth in city staff to align with the growth of Lawrence over the next 50 years with an estimated 355 full-time and 21 part-time personnel.

There will be at least one new roadway connection to public streets with a major access point connecting to the intersection of E 19th Street \& O'Connell Road. Although the current orientation of buildings and circulation roadway within the campus is still under development, an additional roadway access connection is being considered for either Greenway Circle and/or E 15th Street to meet emergency service access requirements. The intersection of E 19th Street \& O'Connell Road will be reconfigured into a stop-controlled T-intersection with O'Connell Road extending to the north.


Site Location Map, Lawrence, Kansas

Many of the vacated improvements currently on site will be removed, including Tank 5 and Tank 6. The bulk warehouse and bag warehouse buildings are planned to remain unchanged due to this development but other options are being discussed at this time. Additional details for the existing site conditions are shown in the image below.


Existing Conditions Site Map, Lawrence, Kansas

The overall objective of the report is to look at proposed land uses and nearby intersections to determine if additional improvements are needed based on trip generation levels. The report will provide details on planned site improvements, provide traffic generation volumes, use available traffic data to distribute volumes for peak hour analysis, provide a Synchro analysis using performance measures, analyze multi-modal aspects of the facility, and provide details on the proposed roadways and access points.

## Section 1: Specific Development Plan and Land Use

Land Use of Development: The land use for the site will be converted from the "Former Farmland/Vacant" category to "Institution" category. The site includes portions of two parcels currently owned by the City of Lawrence, Parcel ID 102-04-0-00-00-002.01-0 and Parcel ID

102-04-0-00-02-002.00-0. New improvements to Parcel ID 102-04-0-00-00-002.01-0 will include 3-6 combined-use buildings, bulk storage, fueling station, new roadways, and parking. New improvements to Parcel ID 102-04-0-00-02-002.00-0 will include a roadway connection or other improvements, such as the Household Hazardous Waste (HHW) building, depending on the final building footprint arrangement.


Land Use Map, Lawrence, Kansas

There will be 3 distinct land uses for the development which include the following:
(1) Office and Maintenance Combined Campus
(a) This includes several related-use buildings, offices, conference rooms, workshops, garages, storage bays, a refueling pump, and other building elements needed for city operations. Divisions within the Office and Maintenance Campus include the central maintenance garage, construction management engineering division, facility maintenance, forestry, horticulture, inspections, stormwater, streets, traffic division, wastewater collections, and water distribution.
(b) For trip generation purposes, operating hours are Monday through Friday. It was estimated that $95 \%$ of the employees make at least one additional trip throughout the day if not two. Most employees will arrive around 6:30am, leave between

6:45am-7:00am to go to their scheduled field work, and return to the campus around $5: 00 \mathrm{pm}-5: 15 \mathrm{pm}$. About $50 \%$ of staff will return for lunch around 11:30am-12:00pm. Inspectors leave for the field around 8:00am and return at $5: 00 \mathrm{pm}$. Some of the supervisory staff may make 3 or 4 trips throughout the day for meetings. Maintenance operations hours are 7:30am to $3: 30 \mathrm{pm}$ with cart delivery trucks and maintenance trucks entering and exiting the shop area throughout the day.
(2) Solid Waste Division
(a) This includes trash truck operations.
(b) For trip generation purposes, operation hours are slightly different than Office and Maintenance operations since trash trucks operate Monday through Saturday. About 70\% of the collection services operation starts at 6:00am with the other $30 \%$ at 7:00am. There is a single "late truck" that starts at 7:30am. Trucks leaving at 6:00am are expected to return back from their route at around $2: 00-2: 15 \mathrm{pm}$ to be clocked out by $2: 30 \mathrm{pm}$. Trucks leaving at 7:00am are expected to return back from their route at around $3: 00-3: 15 \mathrm{pm}$ to be clocked out by $3: 30 \mathrm{pm}$. The single "late truck" works until 4:00pm. Inclement weather slows down operations as well as when students move out meaning that, on occasion, the 6:00am trucks don't return until 3:00-3:30pm. Only 3 trucks run on Saturdays with a start time of 6:00am and ending around 12:00pm.
(3) Household Hazardous Waste
(a) This includes household hazardous waste operations as well as a drop-off area for the public. This building will be outside of the fenced-in section of the campus.
(b) For trip generation purposes, the facility is open to the public $8: 00 \mathrm{am}-1: 00 \mathrm{pm}$ Tuesday, Wednesday, and Thursday. The number of public trips is expected to be 7 per hour.

Land Use of Surrounding Properties: To the north, across the BNSF Railroad rail line, the land use category is Agriculture. To the east, the land use category is Industrial. To the south of the site is vacant which is undeveloped/partially developed. To the west of the site, the land use categories are Vacant on the southside of E 19th Street and Multiple Family Residential on the northside of E 19th Street.

Development Plan: The following Facility Divisions will share space in the new campus:

- CMG - Central Maintenance Garage
- Service and repair for all City-owned equipment
- 73,770 sq ft for Main Building, 8.25 acres for total site requirements
- 17 full-time employees
- CMED - Construction Management Engineering Division
- Engineering oversight and management for construction projects in the City
- $8,490 \mathrm{sq} \mathrm{ft}$ for Main Building, 2.71 acres for total site requirements
- 14 full-time employees
- FAC - Facility Maintenance Division
- Maintenance and operations for 258 City-owned buildings/structures and grounds
- 33,523 sq ft for Main Building, 4.60 acres for total site requirements
- 10 full-time employees and 1 part-time employee
- FOR - Forestry Division
- Protect and maintain street trees
- 24,665 sq ft for Main Building, 2.70 acres for total site requirements
- 5 full-time employees and 3 part-time employee
- HOR - Horticulture Division
- Maintenance of landscaping and natural areas
- $11,856 \mathrm{sq} \mathrm{ft}$ for Main Building, 10.52 acres for total site requirements
- 5 full-time employees and 5 part-time employee
- HHW - Household Hazardous Waste Division
- City and County drop off location for household hazardous waste
- 12,181 sq ft for Main Building, 2.78 acres for total site requirements
- 1 full-time employee and 4 part-time employees
- INS - Inspections Division
- Inspection of construction and repair projects
- $4,713 \mathrm{sq} \mathrm{ft}$ for Main Building, 1.93 acres for total site requirements
- 9 full-time employees
- SWD - Solid Waste Division
- Collection of trash, recycling, yard waste, bulky items and tires
- $43,584 \mathrm{sq} \mathrm{ft}$ for Main Building, 14.48 acres for total site requirements
- 80 full-time employees
- STWT - Stormwater Division
- Stormwater system oversight and management
- $51,623 \mathrm{sq} \mathrm{ft}$ for Main Building, 6.56 acres for total site requirements
- 10 full-time employees
- STRT - Streets Division
- Roadway oversight and management
- 79,626 sq ft for Main Building, 11.93 acres for total site requirements
- 24 full-time employees
- TRAF - Traffic Division
- Street signage and intersection traffic signal oversight and management
- 23,513 sq ft for Main Building, 3.16 acres for total site requirements
- 6 full-time employees
- WSWT - Wastewater Collections Division
- Sanitary sewer system oversight and management
- 22,729 sq ft for Main Building, 2.53 acres for total site requirements
- 10 full-time employees
- WTDT - Water Distribution Division
- Water distribution system oversight and management
- 58,583 sq ft for Main Building, 10.00 acres for total site requirements
- 32 full-time employees

For the Office and Maintenance Combined Campus including the Household Hazardous Waste division, the total building square footage is $448,856 \mathrm{sq} \mathrm{ft}$ and the total acreage is 82.15 acres. The final building layout is being refined at the time of writing this report. The general concept of the buildings is shown in the image below.


Schematic Building Layout

## Section 2: Land Use Shown in the Lawrence/Douglas County Comprehensive Plan

Land Uses in the Lawrence/Douglas County Comprehensive Plan: The land use shown in the Plan 2040 GIS maps show that the site is partially vacant and partially industrial.


Plan 2040 Industrial Map (Purple)

Shown below are the nearby commercial areas and flood areas which will not be impacted by the new development.


Plan 2040 Commercial Map (Blue)


Plan 2040 Flood Zone Map (Red)

There is no conflict between the proposed land use for the new development and the Comprehensive Plan.

## Section 3: Functional Classification of the Public Streets Bordering the Site

Surrounding Public Streets and Highway Network: As shown in the Transportation 2040 (T2040) report developed by the Metropolitan Transportation Plan of Lawrence and Douglas County, the functional classification of the surrounding streets is shown in the map below.


Roadway Functional Classification Map

Surrounding Roadways include the following:

- E 23rd Street/N 1400 Road - Principal Arterial
- O'Connell Road/E 1600 Road - Collector/Rural Major Collector
- Venture Park Drive - Collector/Rural Major Collector
- Greenway Circle - Collector/Rural Major Collector
- Noria Road/E 1750 Road - Minor Arterial
- E 19th Street - Collector/Rural Major Collector
- Harper Street - Collector/Rural Major Collector


## Section 4: Access to the Development, Internal Circulation, and Truck Turning Movements

Access to the Development: The main access to the development will be an extension of O'Connell Road to the north of 19th Street. North of O'Connell Road \& 19th Street will be a security gate entrance. The roadway will provide internal circulation through the site and will be used by vehicles traveling between buildings, vehicle maintenance bays, and workshops. Several options for a back entrance are being considered as an alternative egress for emergency/fire access.


Potential Layout
Internal Circulation and Parking: The final parking lot layout and circulation plan is being refined at the time of writing this report. The general concept of vehicle flow is shown in the image below.


The Facility Divisions within the campus will share parking spaces although parking space requirements per division have been calculated separately to ensure parking needs are satisfied. The number of vehicle parking spaces is outlined below:

- CMG - Central Maintenance Garage
- Staff Parking - 30 spaces
- ADA Reserved Parking - 1 space
- Conditioned Vehicle Storage (Warm) - 3,366 sq ft total
- Pickup - 6 spaces at $10 \mathrm{ft} \times 20 \mathrm{ft}$
- Large Service Bays - 18 spaces at $28 \mathrm{ft} x 52 \mathrm{ft}$
- Small Service Bays - 12 spaces at $22 \mathrm{ft} \times 32 \mathrm{ft}$
- Tire Service Bay-1 space at $28 \mathrm{ft} \times 52 \mathrm{ft}$
- Fleet Staging Area - 6 spaces at $20 \mathrm{ft} \times 45 \mathrm{ft}$
- Wash Bay - 1 space at $30 \mathrm{ft} \times 56 \mathrm{ft}$
- Fuel Island - 1 space at $30 \mathrm{ft} \times 50 \mathrm{ft}$
- Trash / Recycling Area - 1 space at $30 \mathrm{ft} \times 30 \mathrm{ft}$
- CMED - Construction Management Engineering Division
- Staff Parking - 23 spaces
- ADA Reserved Parking - 1 space
- Exterior Equipment Parking - 10 spaces at $12 \mathrm{ft} \times 24 \mathrm{ft}$
- FAC - Facility Maintenance Division
- Staff Parking - 18 spaces
- ADA Reserved Parking - 1 space
- Conditioned Vehicle Storage (Warm) - 26,668 sq ft total

■ Large - 5 spaces at $20 \mathrm{ft} \times 45 \mathrm{ft}$

- Medium - 14 spaces at $12 \mathrm{ft} \times 24 \mathrm{ft}$
- Pickup - 5 spaces at $10 \mathrm{ft} \times 20 \mathrm{ft}$
- Unconditioned Vehicle Storage (Cold) - 8,976 sq ft total

■ Pickup - 16 spaces at $10 \mathrm{ft} \times 20 \mathrm{ft}$

- Trash / Recycling Area - 1 space at $30 \mathrm{ft} \times 30 \mathrm{ft}$
- FOR - Forestry Division
- Staff Parking - 8 spaces
- ADA Reserved Parking - 1 space
- Conditioned Vehicle Storage (Warm) - 19,191 sq ft total
- Large - 5 spaces at $20 \mathrm{ft} \times 45 \mathrm{ft}$
- Medium - 3 spaces at $12 \mathrm{ft} \times 24 \mathrm{ft}$
- Pickup - 8 spaces at $10 \mathrm{ft} \times 20 \mathrm{ft}$
- Unconditioned Vehicle Storage (Cold) - 1,795 sq ft total
- Pickup - 3 spaces at $10 \mathrm{ft} \times 20 \mathrm{ft}$
- Trash / Recycling Area - 1 space at 30 ft x 30 ft
- HOR - Horticulture Division
- Staff Parking - 26 spaces
- ADA Reserved Parking - 1 space
- Conditioned Vehicle Storage (Warm) - 4,825 sq ft total
- Pickup - 9 spaces at $10 \mathrm{ft} \times 20 \mathrm{ft}$
- Unconditioned Vehicle Storage (Cold) - 8,976 sq ft total
- Pickup - 16 spaces at $10 \mathrm{ft} \times 20 \mathrm{ft}$
- Exterior Equipment Parking - 14 spaces at $12 \mathrm{ft} \times 24 \mathrm{ft}$
- Trash / Recycling Area - 1 space at 30 ft x 30 ft
- HHW - Household Hazardous Waste Division
- Staff Parking - 9 spaces
- ADA Reserved Parking - 2 spaces
- Visitor Parking - 17 spaces
- Visitor Drive-thru-1 space at 15 ft x 15 ft
- Conditioned Vehicle Storage (Warm) - 561 sq ft total
- Pickup - 1 spaces at $10 \mathrm{ft} \times 20 \mathrm{ft}$
- Household Hazardous Waste Dumpster Containers - 3 spaces at $8 \mathrm{ft} x 13 \mathrm{ft}$
- INS - Inspections Division
- Staff Parking - 15 spaces
- ADA Reserved Parking - 1 space
- Exterior Equipment Parking - 14 spaces at $12 \mathrm{ft} \times 24 \mathrm{ft}$
- SWD - Solid Waste Division
- Staff Parking - 109 spaces
- ADA Reserved Parking - 4 spaces
- Exterior Equipment Parking - 109 spaces at $12 \mathrm{ft} \times 24 \mathrm{ft}$
- Wash Bay - 2 spaces at $30 \mathrm{ft} \times 56 \mathrm{ft}$
- Fuel Island - 1 space at $30 \mathrm{ft} \times 50 \mathrm{ft}$
- Dumpster and Cart Storage Area - 1 space at $160 \mathrm{ft} \times 300 \mathrm{ft}$
- STWT - Stormwater Division
- Staff Parking - 16 spaces
- ADA Reserved Parking - 1 space
- Conditioned Vehicle Storage (Warm) - 39,898 sq ft total
- Large - 13 spaces at $20 \mathrm{ft} \times 45 \mathrm{ft}$
- Medium - 8 spaces at $12 \mathrm{ft} \times 24 \mathrm{ft}$
- Pickup - 2 spaces at $10 \mathrm{ft} \times 20 \mathrm{ft}$
- Unconditioned Vehicle Storage (Cold) - 12,629 sq ft total
- Medium - 5 spaces at $12 \mathrm{ft} \times 24 \mathrm{ft}$
- Pickup - 16 spaces at $10 \mathrm{ft} \times 20 \mathrm{ft}$
- Exterior Equipment Parking - 13 spaces at $12 \mathrm{ft} \times 24 \mathrm{ft}$
- Wash Bay - 1 space at $30 \mathrm{ft} \times 56 \mathrm{ft}$
- STRT - Streets Division
- Staff Parking - 39 spaces
- ADA Reserved Parking - 2 spaces
- Conditioned Vehicle Storage (Warm) - $61,055 \mathrm{sq} \mathrm{ft}$ total
- Large - 19 spaces at $20 \mathrm{ft} \times 45 \mathrm{ft}$
- Medium - 13 spaces at $12 \mathrm{ft} \times 24 \mathrm{ft}$
- Pickup - 4 spaces at $10 \mathrm{ft} \times 20 \mathrm{ft}$
- Unconditioned Vehicle Storage (Cold) - 11,561 sq ft total
- Medium - 3 spaces at $12 \mathrm{ft} \times 24 \mathrm{ft}$
- Pickup - 16 spaces at $10 \mathrm{ft} \times 20 \mathrm{ft}$
- Exterior Equipment Parking - 28 spaces at $12 \mathrm{ft} \times 24 \mathrm{ft}$
- Wash Bay - 1 space at 30 ft x 56 ft
- Fuel Island-1 space at $30 \mathrm{ft} \times 50 \mathrm{ft}$
- Trash / Recycling Area - 1 space at 30 ft x 30 ft
- TRAF - Traffic Division
- Staff Parking - 10 spaces
- ADA Reserved Parking - 1 space
- Conditioned Vehicle Storage (Warm) - 7,414 sq ft total
- Medium - 6 spaces at $12 \mathrm{ft} \times 24 \mathrm{ft}$
- Pickup - 4 spaces at $10 \mathrm{ft} \times 20 \mathrm{ft}$
- Exterior Equipment Parking - 6 spaces at $12 \mathrm{ft} \times 24 \mathrm{ft}$
- WSWT - Wastewater Collections Division
- Staff Parking - 16 spaces
- ADA Reserved Parking - 1 space
- Conditioned Vehicle Storage (Warm) - 17,126 sq ft total
- Large - 3 spaces at $20 \mathrm{ft} \times 45 \mathrm{ft}$
- Medium-11 spaces at $12 \mathrm{ft} \times 24 \mathrm{ft}$
- WTDT - Water Distribution Division
- Staff Parking - 52 spaces
- ADA Reserved Parking - 2 spaces
- Conditioned Vehicle Storage (Warm) - 37,443 sq ft total
- Large - 6 spaces at $20 \mathrm{ft} \times 45 \mathrm{ft}$
- Medium - 18 spaces at $12 \mathrm{ft} \times 24 \mathrm{ft}$
- Pickup - 13 spaces at $10 \mathrm{ft} \times 20 \mathrm{ft}$
- Unconditioned Vehicle Storage (Cold) - 12,118 sq ft total
- Pickup - 22 spaces at $10 \mathrm{ft} \times 20 \mathrm{ft}$
- Exterior Equipment Parking - 35 spaces at $12 \mathrm{ft} \times 24 \mathrm{ft}$

Truck Turning Movements: Internal circulation routes will provide sufficient space for truck turning maneuvers. Most large trucks are less than 45 ft although the combination of a truck and trailer could be longer. The following image is a draft layout that provides sufficient turning
space for a Lawrence 49 Pumper Fire Truck. A larger version of this illustration has been included in the appendix.


Potential Layout showing Lawrence 49 Pumper Fire Truck Turning Movements

## Section 5: Current Public Street Characteristics Adjacent to the Site

Surrounding Roadways: The following list provides a recap of roadways surrounding the MSO facility.

- E 23rd Street/N 1400 Road - Principal Arterial
- East of O'Connell Road/E 1600 Road
- 4 lane divided roadway with a speed limit of 55 mph
- West of O'Connell Road/E 1600 Road
- 4 lane divided roadway transition to a 5 lane undivided roadway with a speed limit of 45 mph
- O'Connell Road/E 1600 Road - Collector/Rural Major Collector
- South of Venture Park Drive
- 4 lane divided roadway with a speed limit of 35 mph and bike lanes
- North of Venture Park Drive
- 2 lane divided roadway with a speed limit of 35 mph and bike lanes
- Venture Park Drive - Collector/Rural Major Collector
- 2 lane undivided roadway with a speed limit of 35 mph and bike lanes
- Greenway Circle - Collector/Rural Major Collector
- 2 lane undivided roadway with a speed limit of 35 mph
- Noria Road/E 1750 Road - Minor Arterial
- 2 lane undivided roadway with a speed limit of 45 mph
- E 19th Street - Collector/Rural Major Collector
- 2 lane undivided roadway with a speed limit of 30 mph
- Harper Street - Collector/Rural Major Collector
- 2 lane undivided roadway with a speed limit of 35 mph between 19th Street and 23 rd Street, otherwise the speed limit is 30 mph

There are several proposed improvements to surrounding roadways as listed in the T2040 report. The report states that Harper Street, from 15th Street to 19th Street, is planned to be reconstructed. 19th Street, from Harper Street to O'Connell Road, is also planned to be reconstructed in 2021. The reconstruction is necessary due to pavement deterioration and would allow the continuation of bike lanes and sidewalks to match the rest of 19th Street. Future design plans would include curb \& gutter, stormwater improvements, and address the current disconnection between O'Connell Road and 19th Street. T2040 lists the intersection of Harper Street \& 19th Street as a candidate for a roundabout.

Public feedback from the T2040 report included several comments in regards to 19th Street improvements. Due to concerns that 19th Street will experience more traffic and will be treated like an arterial roadway rather than a collector roadway, many residents and representatives of the 19th Street Neighborhoods Coalition question whether connecting O'Connell Road to 19th Street is necessary. Since 19th Street is currently a "No Outlet" collector, the roadway does not experience thru traffic.


Current Condition of O'Connell Road \& 19th Street

The public feedback centers on the potential level of traffic in conflict with walkability goals and neighborhood safety. This report does not cover any further detail of the future design of 19th Street improvements. If 19th Street is connected to O'Connell Road, some new trips generated by the MSO Facility might utilize 19th Street for emergency vehicle service, trash truck service, or other city vehicles in-service to the neighborhood; Most trips to and from the MSO facility will not utilize 19th Street because the layout of the MSO facility's main access drive will be an extension of O'Connell Road and vehicles that utilize O'Connell Road will have a quicker travel time to access a majority of Lawrence. Since 19th Street is not on the City's truck routing map, all trucks will be required to utilize O’Connell Road to get to E 23rd Street.

Water Conflicts: The flood map for the selected area is number 20045C0179E, effective on $09 / 02 / 2015$, showed that the site was located outside of the 500 year flood zone.

Existing Alternative Transportation Mode Choices: Currently, there are sidewalks along both sides of O'Connell Road and Venture Park Drive. There is an existing sidewalk segment on the northside of E 19th Street. There are bicycle lanes on O'Connell Road and Venture Park Drive. Transit buses are routed along O’Connell Road and Venture Park Drive (Routes 5 and 15) and along Harper St and 19th Street (Route 1) which serve the area for the new development.


Bus Routes

Crash Analysis: The analysis of crash data near the vicinity of the MSO Facility was limited to the previous 5 years, January 2014 to December 2018. During the 5 years, all observed crashes occurred along E 23rd Street/N 1400 Road or Venture Park Drive or at the intersections of K-10/E 23rd Street \& O’Connell Road/E 1600 Road and O'Connell Road \& Venture Park Drive.


Crash Locations near the vicinity of the MSO Facility, Jan 2014 to Dec 2018

Details of total crashes are summarized in the tables below:
Table 1. Number of Crashes in Each Year

| Year | \# of Crashes | Percentage |
| :--- | :---: | :---: |
| 2014 | 14 | $12.5 \%$ |
| 2015 | 33 | $29.5 \%$ |
| 2016 | 34 | $30.4 \%$ |
| 2017 | 18 | $16.1 \%$ |
| 2018 | 13 | $11.6 \%$ |
| Grand Total | 112 | $100 \%$ |

Table 2. Number of Crashes per Category | Location Type

| Location Type | \# of Crashes | Percentage | \# of Vehicles | Percentage |
| :--- | :---: | :---: | :---: | :---: |
| INTERSECTION-ON ROAD | 11 | $9.8 \%$ | 23 | $9.8 \%$ |
| INTERSECTION-RELATED-ON ROAD | 66 | $58.9 \%$ | 145 | $62.0 \%$ |
| MEDIAN-OFF ROAD | 2 | $1.8 \%$ | 3 | $1.3 \%$ |
| NON-INTERSECTION-ON ROAD | 31 | $27.7 \%$ | 61 | $26.1 \%$ |
| ROADSIDE-NO SHLDR-OFF ROAD | 2 | $1.8 \%$ | 2 | $0.9 \%$ |
| Grand Total | $\mathbf{1 1 2}$ | $100.0 \%$ | $\mathbf{2 3 4}$ | $100.0 \%$ |

Of the 112 total crashes, $58.9 \%$ occurred on a roadway related to the presence of an intersection, $27.7 \%$ occurred on a roadway without being related to the presence of an intersection, $9.8 \%$ occurred within an intersection, $1.8 \%$ occurred off of a roadway within the median, and $1.8 \%$ occurred within the roadside.

Table 3. Number of Crashes per Category | Collision Type

| Collision Type | \# of Crashes | Percentage | \# of Vehicles | Percentage |
| :--- | :---: | :---: | :---: | :---: |
| WITH ANIMAL | 3 | $2.7 \%$ | 3 | $1.3 \%$ |
| WITH FIXED OBJECT | 8 | $7.1 \%$ | 9 | $3.8 \%$ |
| WITH OTHER MOTOR VEHICLE | 99 | $88.4 \%$ | 220 | $94.0 \%$ |
| WITH PEDESTRIAN | 2 | $1.8 \%$ | 2 | $0.9 \%$ |
|  | 112 | $100.0 \%$ | 234 | $100.0 \%$ |

Of the 112 total crashes, $88.4 \%$ occurred with at least one other motor vehicle, $7.1 \%$ occurred with fixed objects, $2.7 \%$ occurred with animals, and $1.8 \%$ occurred with pedestrians.

Table 4. Number of Vehicles | Location Type vs Collision Type

| Location Type vs Collision Type | WITH <br> ANIMAL | WITH FIXED <br> OBIECT | WITH OTHER <br> MOTOR <br> VEHICLE | WITH <br> PEDESTRIAN | Grand Total |
| :--- | :---: | :---: | :---: | :---: | :---: |
| INTERSECTION-ON ROAD |  | 1 | 22 |  | 23 |
| INTERSECTION-RELATED-ON ROAD |  | 1 | 144 |  | 145 |
| MEDIAN-OFF ROAD |  | 3 |  |  | 3 |
| NON-INTERSECTION-ON ROAD | 3 | 2 | 54 | 2 | 61 |
| ROADSIDE-NO SHLDR-OFF ROAD |  | 2 |  | 2 | 234 |
| Grand Total | $\mathbf{3}$ | 9 | 220 | 2 | 234 |

The table above illustrates the total number of vehicles when considering location type and collision type. The two pedestrian crashes occurred on the roadway not at an intersection.

Table 5. Number of Crashes per Category | Lighting Conditions

| Lighting Conditions | \# of Crashes | Percentage | \# of Vehicles | Percentage |
| :--- | :---: | :---: | :---: | :---: |
| DARK--NO STREET LIGHTS | 3 | $2.7 \%$ | 5 | $2.1 \%$ |
| DARK--STREET LIGHTS ON | 18 | $16.1 \%$ | 35 | $15.0 \%$ |
| DAWN | 4 | $3.6 \%$ | 9 | $3.8 \%$ |
| DAYLIGHT | 84 | $75.0 \%$ | 177 | $75.6 \%$ |
| DUSK | 3 | $2.7 \%$ | 8 | $3.4 \%$ |
|  | $\mathbf{~ G r a n d ~ T o t a l ~}$ | 112 | $100 \%$ | $\mathbf{2 3 4}$ |

Of the 112 total crashes, $75 \%$ occurred during daylight hours, $16.1 \%$ occurred during dark with street lights turned on, $2.7 \%$ occurred during dark without street lights, $3.6 \%$ occurred during dawn, and $2.7 \%$ occurred during dusk.

Table 6. Number of Crashes per Category | Weather Conditions

| Weather Conditions | \# of Crashes | Percentage | \# of Vehicles | Percentage |
| :--- | :---: | :---: | :---: | :---: |
| FOG | 2 | $1.8 \%$ | 4 | $1.7 \%$ |
| FREEZING RAIN | 1 | $0.9 \%$ | 3 | $1.3 \%$ |
| NO ADVERSE CONDITIONS | 94 | $83.9 \%$ | 196 | $83.8 \%$ |
| RAIN, MIST, OR DRIZZLE | 14 | $12.5 \%$ | 29 | $12.4 \%$ |
| SNOW | 1 | $0.9 \%$ | 2 | $0.9 \%$ |
|  | 112 | $100 \%$ | 234 | $100.0 \%$ |

Of the 112 total crashes, $83.9 \%$ occurred during no adverse conditions, $12.5 \%$ occurred during rain, mist or drizzle, $1.8 \%$ occurred during fog, $0.9 \%$ occurred during snow, and $0.9 \%$ occurred during freezing rain.

Table 7. Number of Crashes per Category | Crash Type

| Crash Type | \# of Crashes | Percentage | \# of Vehicles | Percentage |
| :--- | :---: | :---: | :---: | :---: |
| UNKNOWN | 13 | $11.6 \%$ | 14 | $6.0 \%$ |
| ANGLE - SIDE IMPACT | 10 | $8.9 \%$ | 20 | $8.5 \%$ |
| HEAD ON | 1 | $0.9 \%$ | 2 | $0.9 \%$ |
| REAR END | 83 | $74.1 \%$ | 186 | $79.5 \%$ |
| SIDESWIPE: SAME DIRECTION | 5 | $4.5 \%$ | 12 | $5.1 \%$ |
| Grand Total | 112 | $100 \%$ | 234 | $100.0 \%$ |

Of the 112 total crashes, $74.1 \%$ involved a rear end, $8.9 \%$ involved an angle-side impact, $4.5 \%$ involved a sideswipe in the same direction, $0.9 \%$ involved a head on, and $11.6 \%$ where left unknown.

Table 8. Severity Distribution per Crash Type

| Crash Type | \# of Crashes | \# of Injury | Percentage | \# of PDO | Percentage |
| :--- | :---: | :---: | :---: | :---: | :---: |
| UNKNOWN | 13 | 3 | $23.1 \%$ | 10 | $76.9 \%$ |
| ANGLE - SIDE IMPACT | 10 | 4 | $40.0 \%$ | 6 | $60.0 \%$ |
| HEAD ON | 1 | 0 | $0.0 \%$ | 1 | $100.0 \%$ |
| REAR END | 83 | 17 | $20.5 \%$ | 66 | $79.5 \%$ |
| SIDESWIPE: SAME DIRECTION | 5 | 1 | $20.0 \%$ | 4 | $80.0 \%$ |
| Grand Total | 112 | 25 | $22.3 \%$ | 87 | $77.7 \%$ |

Most of the collisions are clustered around E 23rd Street/N 1400 Road \& O'Connell Road with $74.1 \%$ rear end crashes. Of the 25 injury crashes, most were rear end crashes; however, if an angle/side impact crash occurred, the probability of an injury increased. Head on collisions are rare and the only recorded head-on was at a low enough speed so that there were no injuries. Based on the existing traffic crashes and new trips generated by the MSO facility, no improvements of the surrounding roadway network are recommended at this time.

## Section 6: Proposed Access Compared with Design Criteria and Sight Distance Requirements

For the proposed access locations, the design speed is 35 mph resulting in a required stopping sight distance of 250 ft and an intersection sight distance of 390 ft . Although the layout of the access drives are currently under design consideration, the sight distance requirements given the current layout of the existing roadways is met. The new access drives will be laid out to meet these design constraints.

## Section 7: Estimate of Trips Generated by Existing and Proposed Development

Existing Trip Generation: No trips are currently generated by the current land use.

Proposed Trip Generation: Since the City of Lawrence has defined how many employees will be working within each division and when they are expected to arrive and depart throughout the day, the number of trips can be estimated.

| Trip Generation Summary |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{array}{\|c\|} \text { TOTAL } \\ \text { DIVISIONS } \end{array}$ | $\begin{gathered} \text { BUILDING } \\ \text { FLOOR } \\ \text { AREA } \\ (\mathrm{sq} \mathrm{ft}) \end{gathered}$ | $\begin{gathered} \text { TOTA } \\ \text { L SITE } \\ \text { (acres) } \end{gathered}$ | STAFF SUBCATEGOR Y | OPERATING <br> DAYS OF <br> THE WEEK | APPROX. OPERATING HOURS |
| Office and <br> Maintenance <br> Combined <br> Campus <br> (Staff) | 11 | 393,091 | 65 | Campus-only Staff | MON-FRI | $\begin{gathered} 7: 00 \mathrm{am}- \\ 5: 00 \mathrm{pm} \end{gathered}$ |
|  |  |  |  | Site Visiting Staff | MON-FRI | $\begin{gathered} \text { 6:30am - } \\ 5: 00 \mathrm{pm} \end{gathered}$ |
|  |  |  |  | Inspectors | MON-FRI | $\begin{gathered} \hline 8: 00 \mathrm{am}- \\ 5: 00 \mathrm{pm} \end{gathered}$ |
|  |  |  |  | Maintenance Staff | MON-FRI | $\begin{gathered} 7: 30 \mathrm{am}- \\ 3: 30 \mathrm{pm} \end{gathered}$ |
| Solid Waste <br> Division <br> (Staff) | 1 | 43,584 | 14 | Fleet Round 1 | MON-SAT | $\begin{gathered} \text { 6:00am - } \\ \text { 2:00pm } \end{gathered}$ |
|  |  |  |  | Fleet Round 2 | MON-SAT | $\begin{gathered} 7: 00 \mathrm{am}- \\ \text { 3:00pm } \end{gathered}$ |
|  |  |  |  | Fleet Round 3 | MON-SAT | $\begin{gathered} \text { 7:30am - } \\ \text { 4:00pm } \end{gathered}$ |
| Household <br> Hazardous <br> Waste (Staff) | 1 | 12,181 | 3 | Campus-only Staff | MON-FRI | $\begin{gathered} \text { 6:30am - } \\ 5: 00 \mathrm{pm} \end{gathered}$ |
| Household <br> Hazardous <br> Waste (Public <br> Drop Off) |  |  |  | Public | TUES-THUR | $\begin{gathered} \text { 8:00am - } \\ \text { 1:00pm } \end{gathered}$ |


| Trip Generation Summary 2020 |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | NUMBER OF EMPLOYEES |  | EXPECTED DAILY TRIPS PER STAFF SUBCATEGORY (Veh / Day Employee) | ESTIMATED <br> DAILY <br> TRIPS (Veh / Day) | $\begin{aligned} & \text { A.M. PEAK } \\ & \text { HOUR, } \\ & \text { 7-9am (Veh } \\ & \text { / Hour) } \end{aligned}$ |  | $\begin{aligned} & \text { P.M. PEAK } \\ & \text { HOUR, } \\ & \text { 4-6pm (Veh } \\ & \text { / Hour) } \end{aligned}$ |  |
|  | (Full and Part Time) |  |  |  | IN | OUT | IN | OUT |
| Office and <br> Maintenance <br> Combined <br> Campus <br> (Staff) | 8 | Employees | 2 | 16 | 8 |  |  | 8 |
|  | 117 | Employees | 6 | 702 | 117 | 117 | 117 | 117 |
|  | 9 | Employees | 8 | 72 | 9 | 9 | 9 | 9 |
|  | 17 | Employees | 2 | 34 | 17 |  |  | 17 |
| Solid Waste <br> Division <br> (Staff) | 56 | Employees | 2 | 112 |  |  |  |  |
|  | 23 | Employees | 2 | 46 | 23 | 23 |  |  |
|  | 1 | Employee | 2 | 2 | 1 | 1 | 1 | 1 |
| Household <br> Hazardous <br> Waste (Staff) | 5 | Employees | 2 | 10 | 5 |  |  | 5 |
| Household <br> Hazardous <br> Waste (Public <br> Drop Off) |  |  |  | 35 | 7 | 7 |  |  |
| Total | 236 | Employees |  | 1029 | 187 | 157 | 127 | 157 |

Verification of Trip Generation Rates and Design Hour Volume Data: To verify the trips produced by the proposed development, trip generation volumes were compared utilizing the land use types categorized by the Institute of Transportation Engineer's Trip Generation Guidelines, 10th Edition. "Government Office Complex" (ITE Code 733) and "Utility" (ITE Code 170) were the ITE Land Use categories used to compare against the expected trips for the campus. The estimated number of trips were based on the number of employees. Copies of the applicable ITE Trip Generation Manual pages are included in the appendix. The following tables show the parameters for measurement units, total trip generation rates for peak hour traffic volumes, and corresponding total vehicles for peak hour traffic at the site.

ITE Traffic Generation Parameters Comparison Chart

| ITE Category | Government Office <br> Complex <br> (ITE Code 733) | Utility <br> (ITE Code 170) | Expected Trips <br> (Based on City-Provided <br> Data) |
| :---: | :---: | :---: | :---: |
| Weekday Total | 13.29 | 4.11 | 4.36 |
| Weekday In | $50 \%$ | $50 \%$ | $50 \%$ |
| Weekday Out | $50 \%$ | $50 \%$ | $50 \%$ |
| Peak Hour of Adjacent Street Traffic, One Hour |  |  |  |
| AM Peak Total | 0.83 | 0.70 | 0.70 |
| AM Peak In | $89 \%$ | $81 \%$ | $81 \%$ |
| AM Peak Out | $11 \%$ | $19 \%$ | $19 \%$ |
| PM Peak Total | 1.10 | 0.76 | 0.76 |
| PM Peak In | $31 \%$ | $15 \%$ | $15 \%$ |
| PM Peak Out | $69 \%$ | $85 \%$ | $85 \%$ |

ITE Traffic Generation Volumes Comparison Chart

| ITE Category | Government Office <br> Complex <br> (ITE Code 733) | Utility <br> (ITE Code 170) | Expected Trips <br> (Based on City-Provided <br> Data) |
| :---: | :---: | :---: | :---: |
| Units | Employee | Employee | Employee |
| Expected Units | 236 | 236 | 236 |
| Weekday Total | 3,136 | 970 | 1,029 |
| Weekday In | 1,568 | 485 | 514.5 |
| Weekday Out | 1,568 | 485 | 514.5 |
| AM Peak Total | 196 | 165 | 344 |
| AM Peak In | 174 | 134 | 187 |
| AM Peak Out | 22 | 31 | 157 |
| PM Peak Total | 260 | 179 | 284 |
| PM Peak In | 80 | 27 | 127 |
| PM Peak Out | 179 | 152 | 157 |

The expected trips most closely resemble trip generation parameters for the Utility category with only a slight increase in volume ( $6 \%$ difference).

Reductions for Pass-By and Diverted-Link Trips: The land-use is not applicable to pass-by trip generation. No diverted-link analysis was done for this analysis.

## Section 8: Traffic Data

Existing Traffic Volumes: Traffic count data was provided at the intersection of E 23rd Street/N 1400 Road \& O’Connell Road/E 1600 Road on Tuesday, December 3, 2019. Although this study occurred during the COVID-19 pandemic, which caused a drastic change in traffic volumes, the data used for the analysis was taken December 3rd, 2019 well before the event. Counts were taken over a 24 -hour period and were recorded in 15 minutes intervals. Recorded vehicle classifications included the following: light vehicles (motorcycles, cars, and light goods vehicles), buses and single-unit trucks, articulated trucks, bikes on the crosswalk, and pedestrians on the crosswalk. Inclement weather conditions or national holiday traffic did not impact the traffic counts.

The combined daily traffic through the intersection was $20,475 \mathrm{vpd}$. There are $1,037 \mathrm{vpd}$ currently using O'Connell Road/E 1600 Road to the north of E 23rd Street/N 1400 Road. With the new trips from the MSO facility, the daily trips are expected to grow to about 2,000 vpd.

For the AM Peak, between 7:45AM - 8:45 AM, all trips headed toward the new development came from the west or south meaning that existing commuters entering the Venture Park area from the east are not likely to use O'Connell Road. On O'Connell Road/E 1600 Road to the north of E 23rd Street/N 1400 Road, there were 45 trips headed northbound and 47 trips headed southbound. The AM peak hour factor was 0.938 .

For the PM Peak, between 4:45PM - 5:45 PM, there were not many vehicles headed toward the new development using O'Connell Road. On O’Connell Road/E 1600 Road to the north of E 23rd Street/N 1400 Road, there were 18 trips headed northbound and 65 trips headed southbound. The PM peak hour factor was 0.953 .

The following tables summarize the daily traffic volumes and AM and PM peak hour traffic volumes:

|  | Daily Total, E 23rd Street \& O’Connell Road Turning Movement Counts |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Existing | 307 | 8583 | 774 | 398 | 8357 | 17 | 826 | 85 | 482 | 19 | 112 | 515 |



|  | AM Peak Hour, E 23rd Street \& O'Connell Road Turning Movement Counts |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Existing | 30 | 593 | 45 | 9 | 552 | 0 | 92 | 15 | 54 | 3 | 3 | 41 |



|  | PM Peak Hour, E 23rd Street \& O’Connell Road Turning Movement Counts |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Existing | 12 | 769 | 94 | 69 | 723 | 4 | 53 | 3 | 31 | 2 | 16 | 47 |



Average Daily Traffic Volumes: An estimate of the average daily traffic on the connecting roadway segments between each intersection is given below:

Based on Dec 3rd, 2019 traffic counts

1. E 23 rd Street/N 1400 Road (East of O'Connell Road/E 1600 Road) $\quad$ ADT $=17,859 \mathrm{vpd}$
2. E 23 rd Street/N 1400 Road (West of O’Connell Road/E 1600 Road) ADT $=19,409 \mathrm{vpd}$
3. O'Connell Road/E 1600 Road (South of E 23 rd Street/N 1400 Road) $\mathrm{ADT}=2,675 \mathrm{vpd}$
4. O'Connell Road/E 1600 Road (North of E 23 rd Street/N 1400 Road) $A D T=1,037 \mathrm{vpd}$
a. Expected ADT post-development construction
$\mathrm{ADT}=2,000 \mathrm{vpd}$

Based on 2016 KDOT traffic counts
5. Harper Street (South of E 19th Street)
$\mathrm{ADT}=5,460 \mathrm{vpd}$
6. E 19th Street (West of Harper Street)

ADT $=3,840 \mathrm{vpd}$
7. Noria Road/E 1750 Road (North of Greenway Circle)

ADT $=4,435 \mathrm{vpd}$


2016 KDOT traffic counts

Buses and Single-unit Trucks: For Buses and Single-unit Trucks, there were a total of 646 vehicles for the 24 hour period making up $3.2 \%$ of total traffic. For the daily total, the highest percentage per movement were EBL and NBL. On O'Connell Road/E 1600 Road to the north of E 23rd Street/N 1400 Road, there were 114 Bus and Single-unit Truck trips making up $11 \%$ of the total traffic on the roadway. The tables below show the amount of Buses and Single-unit Trucks per movement:

|  | Daily Total, E 23rd Street \& O’Connell Road Turning Movement Counts |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Existing | 50 | 200 | 47 | 4 | 163 | 0 | 113 | 1 | 6 | 1 | 5 | 56 |
| Percentage \% | 17.3 | 2.3 | 6.1 | 1.0 | 2.0 | 0 | 13.7 | 1.2 | 1.2 | 5.3 | 4.5 | 10.9 |


|  | AM Peak Hour, E 23rd Street \& O'Connell Road Turning Movement Counts |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Existing | 3 | 9 | 9 | 1 | 15 | 0 | 17 | 0 | 1 | 0 | 1 | 6 |
| Percentage \% | 10.0 | 1.5 | 20.0 | 12.5 | 2.7 | 0 | 18.5 | 0 | 1.9 | 0 | 33.3 | 14.6 |


|  | PM Peak Hour, E 23rd Street \& ' Connell Road Turning Movement Counts |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Existing | 3 | 8 | 0 | 0 | 10 | 0 | 4 | 1 | 1 | 0 | 0 | 2 |
| Percentage \% | 27.3 | 1.0 | 0 | 0 | 1.4 | 0 | 7.5 | 33.3 | 3.2 | 0 | 0 | 4.3 |

Articulated Trucks: For Articulated Trucks, there were a total of 198 vehicles for the 24 hour period making up $1.0 \%$ of total traffic. For the daily total, the highest percentage per movement were SBL and EBL. On O'Connell Road/E 1600 Road to the north of E 23rd Street/N 1400 Road, there were 27 Articulated Truck trips making up $2.6 \%$ of the total traffic on the roadway. The tables below show the amount of Articulated Trucks per movement:

|  | Daily Total, E 23rd Street \& O’Connell Road Turning Movement Counts |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Existing | 15 | 90 | 3 | 2 | 68 | 0 | 2 | 0 | 6 | 1 | 2 | 9 |
| Percentage $\%$ | 5.2 | 1.0 | 0.4 | 0.5 | 0.8 | 0 | 0.2 | 0 | 1.2 | 5.3 | 1.8 | 1.7 |


|  | AM Peak Hour, E 23rd Street \& O'Connell Road Turning Movement Counts |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Existing | 0 | 5 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Percentage \% | 0 | 0.8 | 0 | 0 | 0.7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |


|  | PM Peak Hour, E 23rd Street \& O’Connell Road Turning Movement Counts |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Existing | 2 | 3 | 1 | 0 | 4 | 0 | 0 | 0 | 1 | 0 | 0 | 2 |
| Percentage \% | 18.2 | 0.4 | 1.1 | 0 | 0.6 | 0 | 0 | 0 | 3.2 | 0 | 0 | 4.3 |

Bikes on the Crosswalk: There was only one bicyclist observed on December 3rd.

Pedestrians on the Crosswalk: 8 total pedestrians were observed on December 3rd with 5 crossing the east leg and 3 crossing the south leg of the intersection.

Trip Distribution: Trip distribution patterns were determined based on a gravity model using the peak hour counts around the development's surrounding origins and destinations. Directional percentages were applied along entry and exit paths so that trips could be distributed proportionally and are shown in the following figures.


The trip distribution pattern also considered how many trips generated by the development would travel along 19th Street if 19th Street was connected to O'Connell Road. A previous Traffic Impact Study for Venture Park listed up to $30 \%$ of trips generated by the Venture Park
commercial zone to be routed along 19th Street; however, the trip distribution in that report included a lot of unknown assumptions for the area. Based on the MSO facility's land uses and 19th Street not being listed as a truck route, it was determined that a refined representation of potential trip distribution was needed.

The method used to refine the probable trip distribution pattern along 19th Street was the catchment area method. By identifying a catchment area that would likely use 19th Street compared to O'Connell Road, a general percentage of expected vehicles was estimated. The catchment area was evaluated using a shortest travel time method which is not necessarily aligned with the shortest path. Beyond this estimated catchment boundary, trips to and from the MSO facility will be more likely to be routed to and from the site with a strong preference for arterials due to higher speed limits. This means that, outside the boundary, a collector street such as 19th Street would not have a high probability of becoming a main thoroughfare for MSO facility generated trips. With an approximate catchment area of 2.4 sq miles out of the total 34.26 square miles in the City of Lawrence, this could mean about $7 \%$ of new vehicle trips would be likely to use 19th Street. To be conservative in the estimation, it was assumed that $10 \%$ of all new trips generated by the MSO facility would utilize 19th Street compared to O'Connell Road.


Estimated Catchment Area for Vehicles using 19th Street to Access the MSO Facility

Using the conservative estimate that $10 \%$ of the newly generated trips would utilize 19th Street, the trip distribution patterns were adjusted as follows:


Using these trip distribution percentages, the number of vehicles during the peak hours were added to existing traffic volume patterns.


|  | AM Peak Hour, E 23rd Street \& O’Connell Road Turning Movement Counts |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Existing | 30 | 593 | 45 | 9 | 552 | 0 | 92 | 15 | 54 | 3 | 3 | 41 |
| Trip Generated | 78 |  |  |  |  | 66 |  | 19 |  | 64 | 5 | 67 |
| Total | 108 | 593 | 45 | 9 | 552 | 66 | 92 | 34 | 54 | 67 | 8 | 108 |



|  | PM Peak Hour, E 23rd Street \& O'Connell Road Turning Movement Counts |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Existing | 12 | 769 | 94 | 69 | 723 | 4 | 53 | 3 | 31 | 2 | 16 | 47 |
| Trip <br> Generated | 55 |  |  |  |  | 50 |  | 5 |  | 62 | 2 | 64 |
| Total | 67 | 769 | 94 | 69 | 723 | 54 | 53 | 8 | 31 | 64 | 18 | 111 |

Determining the Growth Rate: The U.S. Census Bureau reported that the Lawrence population in 2000 was 80,098 while the population in 2015 was 94,104 . This is an increase in growth of $17.5 \%$. Based on the available census data, the average annual growth rate of Lawrence was calculated to be $1.08 \%$ which represented a constant linear growth derived from the following equation:

Constant \% Growth (2000 to 2015) $=(\text { End Year vpd } / \text { Beginning Year vpd })^{\wedge}(1 /($ End Year-Beginning Year)) - 1

$$
\begin{aligned}
& =(94,104 / 80,098)^{\wedge}(1 /(2015-2000))-1 \\
& =1.08 \% \text { per year }
\end{aligned}
$$

Because the area is expected to grow slightly in traffic volume due to the proposed development and other possible developments, a $1.08 \%$ annual constant percent growth rate was used to project the increase in traffic volume twenty years into the future.

Growth Factor: The growth factor constant was determined as follows:

$$
\begin{aligned}
\text { Growth Factor Constant } & =(1+\text { Constant } \% \text { Growth Rate })^{\wedge} \text { Projected Years } \\
& =(1+0.0108)^{\wedge} 20 \\
& =1.24, \text { for } 20 \text { years growth at } 1.1 \%
\end{aligned}
$$

Projected Traffic Volumes: The 1.24 growth factor was applied to the existing traffic volumes but not the trips generated by the new development or existing developments. The number of trips attracted to the site will not increase or decrease with time, but would increase or decrease if the number of employees was altered.

In the case of the MSO facility, the campus will be constructed to accommodate a growth in city staff to align with the growth of Lawrence over the next 50 years; therefore, the increase of employees needs to be accounted for within the traffic volumes. Since traffic studies typically analyze traffic patterns projected by only two decades to remain relatively accurate, the number of employees at the facility at the 20 year mark post construction needs to be determined.

Based on data provided by city estimates, the future projected estimated staff includes 355 full-time and 21 part-time personnel at the 50 year mark. The increase in the number of employees at the 20 year mark would be about $40 \%$ of the expected increase in employees by the 50 year mark. Therefore, at the 20 year mark, there would be 276 full-time and 16 part-time personnel. Based on these new employee totals, the trip generation table has been updated for the future projected growth in 20 years.

| Trip Generation Summary 2040 |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | NUMBER OF EMPLOYEES |  | EXPECTED DAILY TRIPS PER STAFF SUBCATEGORY (Veh / Day Employee) | ESTIMATED <br> DAILY <br> TRIPS (Veh Day) | $\begin{aligned} & \text { A.M. PEAK } \\ & \text { HOUR, } \\ & \text { 7-9am (Veh } \\ & \text { / Hour) } \end{aligned}$ |  | $\begin{aligned} & \text { P.M. PEAK } \\ & \text { HOUR, } \\ & \text { 4-6pm (Veh } \\ & \text { / Hour) } \end{aligned}$ |  |
|  | (Full and Part Time) |  |  |  | IN | OUT | IN | OUT |
| Office and <br> Maintenance <br> Combined <br> Campus <br> (Staff) | 9 | Employees | 2 | 18 | 9 |  |  | 9 |
|  | 147 | Employees | 6 | 882 | 147 | 147 | 147 | 147 |
|  | 11 | Employees | 8 | 88 | 11 | 11 | 11 | 11 |
|  | 20 | Employees | 2 | 40 | 20 |  |  | 20 |
| Solid Waste <br> Division <br> (Staff) | 69 | Employees | 2 | 138 |  |  |  |  |
|  | 29 | Employees | 2 | 58 | 29 | 29 |  |  |
|  | 1 | Employee | 2 | 2 | 1 | 1 | 1 | 1 |
| Household <br> Hazardous <br> Waste (Staff) | 6 | Employees | 2 | 12 | 6 |  |  | 6 |
| Household <br> Hazardous <br> Waste (Public <br> Drop Off) |  |  |  | 35 | 9 | 9 |  |  |
| Total | 292 | Employees |  | 1273 | 232 | 197 | 159 | 194 |

These trips were then distributed using the same distribution pattern.


|  | AM Peak Hour, E 23rd Street \& O’Connell Road Turning Movement Counts |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Existing | 30 | 593 | 45 | 9 | 552 | 0 | 92 | 15 | 54 | 3 | 3 | 41 |
| Trip <br> Generated | 78 |  |  |  |  | 66 |  | 19 |  | 64 | 5 | 67 |
| Total | 108 | 593 | 45 | 9 | 552 | 66 | 92 | 34 | 54 | 67 | 8 | 108 |
| Future $=$ <br> Existing *1.24 Growth Factor | 37 | 735 | 56 | 11 | 684 | 0 | 114 | 19 | 67 | 4 | 4 | 51 |
| Future Trip Gen. | 97 |  |  |  |  | 81 |  | 23 |  | 80 | 7 | 85 |
| Future Total | 134 | 735 | 56 | 11 | 684 | 81 | 114 | 42 | 67 | 84 | 11 | 136 |



|  | PM Peak Hour, E 23rd Street \& O’Connell Road Turning Movement Counts |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Existing | 12 | 769 | 94 | 69 | 723 | 4 | 53 | 3 | 31 | 2 | 16 | 47 |
| Trip <br> Generated | 55 |  |  |  |  | 50 |  | 5 |  | 62 | 2 | 64 |
| Total | 67 | 769 | 94 | 69 | 723 | 54 | 53 | 8 | 31 | 64 | 18 | 111 |
| Future $=$ <br> Existing <br> *1.24 Growth <br> Factor | 15 | 954 | 117 | 86 | 897 | 5 | 66 | 4 | 38 | 2 | 20 | 58 |
| Future Trip <br> Gen. | 69 |  |  |  |  |  |  |  |  |  |  |  |

Using these traffic volumes, a Synchro analysis was performed to identify any necessary changes to the intersection.

## Section 9: Synchro Analysis of Performance Measures

Creating Synchro Scenarios: Using the traffic counts and the ITE trip generation volumes, six Synchro models were created for the traffic conditions surrounding the site.

- Scenario 1 - Existing street/pre-development conditions, Weekday AM Peak Traffic 2020
- Scenario 2 - Existing street/pre-development conditions, Weekday PM Peak Traffic 2020
- Scenario 3 - Proposed street/after-development conditions, Weekday AM Peak Traffic 2020
- Scenario 4 - Proposed street/after-development conditions, Weekday PM Peak Traffic 2020
- Scenario 5 - Proposed street/after-development conditions, Weekday AM Peak Traffic 2040
- Scenario 6 - Proposed street/after-development conditions, Weekday PM Peak Traffic 2040

Capacity and Level of Service Analysis: Three performance measures commonly used for Traffic Impact Studies are vehicle delay, level-of-service (LOS), and queue length. Vehicle delay is the average delay, in seconds, experienced by one vehicle passing through the intersection. The quality of traffic operation at an intersection is defined through level-of-service (LOS) which consists of assignments of ' $A$ ' for free-flowing conditions through ' $F$ ' for congested conditions. The procedures and methodology for determining the LOS are outlined in the Highway Capacity Manual (HCM 2010), produced by Transportation Research Broad. LOS 'A' through ' C ' is considered acceptable. For intersections, no individual lane should be below LOS D. The 95th percentile queue length is the overall length of a string of stopped vehicles. Note that the queue is reported in the lefttthrulright order. The results of the Synchro models are in the tables below.

Scenarios 1 \& 2 Synchro Results (Existing)

| Performance Measures | AM 2020 | PM 2020 |
| :--- | :---: | :---: |
|  | E 23rd Street \& O'Connell Road |  |
| Delay, s | 21.7 | 26.3 |
| LOS | C | C |
| NB Delay, s | 10.6 | 12.1 |
| L/T+R | $12.7 / 7.8$ | $14.6 / 8.3$ |
| NB LOS | B | B |
| L/T+R | $\mathrm{B} / \mathrm{A}$ | $\mathrm{B} / \mathrm{A}$ |
| NB Queue, ft | $56 / 35$ | $37 / 22$ |
| EB Delay, s | 22.0 | 32.1 |
| L/T/R | $34.3 / 23.0 / 0.1$ | $34.8 / 35.8 / 1.5$ |
| EB LOS | C | C |
| L/T/R | $\mathrm{C} / \mathrm{C} / \mathrm{A}$ | $\mathrm{C} / \mathrm{D} / \mathrm{A}$ |
| EB Queue, ft | $40 / 194 / 0$ | $22 / 291 / 13$ |
| SB Delay, s | 2.2 | 6.0 |
| L/T/R | $12.7 / 20.3 / 0.2$ | $13.5 / 21.6 / 0.3$ |
| SB LOS | A | A |
| L/T/R | $\mathrm{B} / \mathrm{C} / \mathrm{A}$ | $\mathrm{B} / \mathrm{C} / \mathrm{A}$ |
| SB Queue, ft | $6 / 7 / 0$ | $4 / 21 / 0$ |
| WB Delay, s | 26.2 | 23.1 |
| L/T/R | $33.0 / 26.1 / 0$ | C |
| WB LOS | C | $\mathrm{C} / \mathrm{A}$ |

Existing traffic conditions were evaluated for the intersection of E 23rd Street \& O'Connell Road. For AM peak hour traffic, the delay at the intersection was 21.7 sec on average with an overall LOS C. Each of the approaches and turning movements have a LOS C or better. EB and WB left-turns experienced the most delay compared to the other movements; however, this is likely due to the left-turns active before the other movements meaning a left-turning vehicle arriving just after the green phase for left-turns has to wait out nearly a whole cycle length. For PM peak hour traffic, the delay at the intersection was 26.3 sec on average with an overall LOS C. Each of the approaches have a LOS C or better while only EBT and WBL turning movements are at LOS D. Overall, the traffic signal is operating well under current demand and capacity levels. Queue lengths did not exceed the turn lane capacity for any movement.

Scenarios 3 \& 4 Synchro Results (Proposed street/after-development conditions 2020)

| Performance Measures | AM 2020 | PM 2020 |
| :--- | :---: | :---: |
| E 23rd Street \& O'Connell Road |  |  |
| Delay, s | 21.8 | 28.9 |
| LOS | C | C |
| NB Delay, s | 13.6 | 13.0 |
| L/T+R | $15.3 / 11.8$ | $14.8 / 10.6$ |
| NB LOS | B | B |
| L/T+R | $\mathrm{B} / \mathrm{B}$ | $\mathrm{B} / \mathrm{B}$ |
| NB Queue, ft | $57 / 47$ | $37 / 26$ |
| EB Delay, s | 23.5 | 33.3 |
| L/T/R | $53.2 / 19.9 / 0.1$ | $49.2 / 35.8 / 1.5$ |
| EB LOS | C | C |
| L/T/R | $\mathrm{D} / \mathrm{B} / \mathrm{A}$ | $\mathrm{D} / \mathrm{D} / \mathrm{A}$ |
| EB Queue, ft | $135 / 192 / 0$ | $87 / 291 / 13$ |
| SB Delay, s | 6.7 | 7.4 |
| L/T/R | $14.8 / 21.2 / 0.6$ | $15.0 / 21.7 / 0.7$ |
| SB LOS | A | A |
| L/T/R | $\mathrm{B} / \mathrm{C} / \mathrm{A}$ | $\mathrm{B} / \mathrm{C} / \mathrm{A}$ |
| SB Queue, ft | $44 / 14 / 0$ | $42 / 22 / 0$ |
| WB Delay, s | 26.6 | 30.7 |
| L/T/R | $34.2 / 29.6 / 0.2$ | C |
| WB LOS | $\mathrm{C} / \mathrm{C} / \mathrm{A}$ | C |
| L/T/R | $19 / 183 / 1$ | $\mathrm{D} / \mathrm{C} / \mathrm{A}$ |
| WB Queue, ft |  | $85 / 247 / 0$ |

Existing traffic conditions plus trips generated by the new development were evaluated for the intersection of E 23rd Street \& O'Connell Road. For AM peak hour traffic, the delay at the intersection was 21.8 sec on average with an overall LOS C. This is 0.1 sec more than the existing traffic conditions without the new development trips. Each of the approaches and turning movements have a LOS C or better except EB left-turns. EB left-turns experienced the most delay compared to the other movements since there will be an influx of city employees coming from the east to head to the facility. For PM peak hour traffic, the delay at the intersection was 28.9 sec on average with an overall LOS C. This is 2.6 sec more than the existing traffic conditions without the new development trips. Each of the approaches have a LOS C or better while only EBL, EBT, and WBL turning movements are at LOS D. Given the additional traffic volumes, the traffic signal is operating well under expected demand and capacity levels. Based on the number of turning vehicles in the AM and PM, dual left-turn lanes are not justified. Queue lengths did not exceed the turn lane capacity for any movement.

Scenarios 5 \& 6 Synchro Results (Proposed street/after-development conditions 2040)

| Performance Measures | AM 2040 | PM 2040 |
| :--- | :---: | :---: |
|  | E 23rd Street \& O'Connell Road |  |
| Delay, s | 25.6 | 32.6 |
| LOS | C | C |
| NB Delay, s | 14.6 | 14.8 |
| L/T+R | $16.9 / 12.2$ | $17.3 / 11.4$ |
| NB LOS | B | B |
| L/T+R | $\mathrm{B} / \mathrm{B}$ | $\mathrm{B} / \mathrm{B}$ |
| NB Queue, ft | $69 / 55$ | $49 / 32$ |
| EB Delay, s | 26.3 | 37.2 |
| L/T/R | $70.7 / 20.2 / 0.1$ | $64.2 / 39.1 / 2.9$ |
| EB LOS | C | D |
| L/T/R | $\mathrm{E} / \mathrm{C} / \mathrm{A}$ | $\mathrm{E} / \mathrm{D} / \mathrm{A}$ |
| EB Queue, ft | $166 / 252 / 0$ | $122 / 395 / 25$ |
| SB Delay, s | 7.6 | 9.3 |
| L/T/R | $15.9 / 21.7 / 1.4$ | $17.7 / 24.1 / 2.0$ |
| SB LOS | A | A |
| L/T/R | $\mathrm{B} / \mathrm{C} / \mathrm{A}$ | $\mathrm{B} / \mathrm{C} / \mathrm{A}$ |
| SB Queue, ft | $53 / 17 / 5$ | $57 / 29 / 12$ |
| WB Delay, s | 33.4 | 34.6 |
| L/T/R | $34.8 / 37.1 / 1.1$ | $65.8 / 34.2 / 0.5$ |
| WB LOS | C | C |
| L/T/R | $\mathrm{C} / \mathrm{D} / \mathrm{A}$ | $\mathrm{E} / \mathrm{C} / \mathrm{A}$ |
| WB Queue, $\mathbf{f t}$ | $21 / 257 / 8$ | $125 / 358 / 4$ |

Future traffic conditions plus trips generated by the new development were evaluated for the intersection of E 23rd Street \& O'Connell Road. For AM peak hour traffic, the delay at the intersection was 25.6 sec on average with an overall LOS C. This is 3.8 sec more than the existing 2020 traffic conditions with the new development trips. Each of the approaches and turning movements have a LOS C or better except EBL and WBT. For PM peak hour traffic, the delay at the intersection was 32.6 sec on average with an overall LOS C. This is 3.7 sec more than the existing 2020 traffic conditions with the new development trips. Each of the approaches have a LOS C or better except the eastbound approach with a LOS D. The only turning movements with a LOS C or worse are EBL at LOS E, EBT at LOS D, and WBL at LOS E. The traffic signal is operating well under expected demand and capacity levels. Based on the number of turning vehicles in the AM and PM, dual left-turn lanes are still not justified. Queue lengths did not exceed the turn lane capacity for any movement.

## Section 10: Near-term Impact of Development

The roadways surrounding the planned MSO Facility have the capacity to handle the newly generated trips. The intersection of E 23rd Street \& O'Connell Road does not require improvements to handle the new trips since the traffic volumes do not justify dual left-turn lanes and the queue lengths do not exceed the turn lane capacity for any movement.

Since 19th Street is planned to be connected to O'Connell Road in 2021, some city vehicles would utilize 19th Street with an estimate of up to $10 \%$ of newly generated trips by the MSO facility. This means an additional 16 westbound vehicles and 19 eastbound vehicles during the AM peak hour and an additional 16 westbound vehicles and 13 eastbound vehicles during the PM peak hour between Harper Street and O'Connell Road. Although the neighborhood association has raised concerns about thru traffic utilizing 19th Street, the MSO Facility land-uses would not cause a high enough volume to cause congestion or walkability issues along 19th Street and 19th Street will not be utilized as a truck route.

## Section 11: Impact of Development with Existing Traffic Projected 20 Years

For the projected traffic volumes, no changes are required to handle traffic volumes as a result of the MSO Facility. For 2040 traffic volumes, the intersection of E 23rd Street \& O'Connell Road does not require dual left-turn lanes or extended turn lane capacity for any movement.

## Section 12: Summary and Recommendations

Summary: This traffic study covered the impact of the field operations campus in the City of Lawrence, Kansas. The 168 acre site will include several large buildings and will host a staff of 223 people. The total daily trips for the facility is expected to be 1,029 with 187 entering and 157 leaving during the AM peak hour and with 127 entering and 157 leaving during the PM peak hour. These traffic volumes account for the personnel making multiple site trips to and from the facility throughout the day.

New roadway connections will be constructed connecting to public streets with the major access point connecting to the intersection of E 19th Street \& O'Connell Road. Although the current orientation of buildings within the campus is still under development, the site will be contained within a secure fence with only the Household Hazardous Waste located on the outside as a public drop off location. The intersection of E 19th Street \& O'Connell Road will be reconfigured into a stop-controlled T-intersection with O'Connell Road extended to the north. The intersection of E 23rd Street \& O’Connell Road does not require improvements to handle the new trips. If 19th Street is connected to O'Connell Road, an estimated $10 \%$ of newly generated trips might utilize 19th Street. Between Harper Street and O’Connell Road, trip distribution results included an additional 16 westbound vehicles and 19 eastbound vehicles during the AM peak hour and an additional 16 westbound vehicles and 13 eastbound vehicles during the PM peak hour. In general, O’Connell Road and the surrounding roadway network was constructed with the capacity to handle development in the area. The trips generated by the MSO facility do not justify additional roadway improvements besides the necessary changes needed for access to the site.

## Recommendations:

- Construct the access roadways for the development and ensure trucks can maneuver through the circulating parking areas and fuel areas without issues.
- Ensure sight distance requirements are consistent with AASHTO requirements during finalization of the facility layout.
- If 19th Street is connected to O'Connell Road, reconsider the routing for transit buses through the area.
- Install a street light at the intersection of 19th Street \& O’Connell Road to aid in nighttime visibility.


## Government Office Complex

 (733)Vehicle Trip Ends vs: Employees<br>On a: Weekday

Setting/Location: General Urban/Suburban
Number of Studies: 1
Avg. Num of Employees: 173
Directional Distribution: $50 \%$ entering, $50 \%$ exiting
Vehicle Trip Generation per Employee

| Average Rate | Range of Rates | Standard Deviation |
| :---: | :---: | :---: |
| 13.29 | $13.29-13.29$ | . |

Data Plot and Equation Caution - Small Sample Size


## Government Office Complex

(733)

Vehicle Trip Ends vs: Employees
On a: Weekday,
Peak Hour of Adjacent Street Traffic,
One Hour Between 7 and 9 a.m.
Setting/Location:
General Urban/Suburban
Number of Studies: 1
Avg. Num. of Employees: 173
Directional Distribution: $89 \%$ entering, $11 \%$ exiting
Vehicle Trip Generation per Employee

| Average Rate | Range of Rates | Standard Deviation |
| :---: | :---: | :---: |
| 0.83 | $0.83-0.83$ |  |

Data Plot and Equation Caution -- Small Sample Size


## Government Office Complex

(733)

Vehicle Trip Ends vs: Employees
On a: Weekday,
Peak Hour of Adjacent Street Traffic,
One Hour Between 4 and 6 p.m.
Setting/Location: General Urban/Suburban
Number of Sludies: 1
Avg. Num of Employees: 173
Directional Distribution: $37 \%$ entering, $69 \%$ exiting

## Vehicle Trip Generation per Employee

Average Rate
1.10

Data Plot and Equation


## Utility

(170)

# Vehicle Trip Ends vs: Employees <br> On a: Weekday 

## Setting/Location: General Urban/Suburban

Number of Studies: 14
Avg. Num of Employees: 41
Directional Distribution: $50 \%$ entering, $50 \%$ exting
Vehicle Trip Generation per Employee

| Average Rate | Range of Rates | Standard Deviation |
| :---: | :---: | :---: |
| 4.11 | $0.80-22.00$ | 1.99 |

Data Plot and Equation


## Utility <br> (170)

# Vehicle Trip Ends vs: Employees <br> On a: Weekday, <br> Peak Hour of Adjacent Street Traffic, <br> One Hour Between 7 and 9 a.m. <br> Setting/Location: General Urban/Suburban <br> Number of Studies: 14 <br> Avg. Num. of Employees: 45 <br> Directional Distribution: $81 \%$ entering, $19 \%$ exiting 

## Vehicle Trip Generation per Employee

| Average Rate | Range of Rates | Standard Deviation |
| :---: | :---: | :---: |
| 0.70 | $0.18-2.00$ | 0.28 |

## Data Plot and Equation


Utility
$(170)$

Vehicle Trip Ends vs: Employees
On a: Weekday,
Peak Hour of Adjacent Street Traffic,
One Hour Between 4 and 6 p.m.

## Setting/Location: General Urban/Suburban

Number of Studies: 15
Avg. Num of Employees: 83
Directional Distribution: $15 \%$ entering, $85 \%$ exiting

## Vehicle Trip Generation per Employee

Average Rate
Range of Rates
$0.25-3.00$
Standard Deviation
0.19

## Data Plot and Equation



Full Length (12 AM-12 AM (+1))
All Classes (Lights, Articulated Trucks, Buses and Single-Unit Trucks, Pedestrians, Bicycles on Crosswalk) All Movements
ID: 731785, Location: 38.942698, -95.204907


| $\begin{array}{\|l\|} \hline \text { Leg } \\ \text { Direction } \\ \hline \end{array}$ | 1600 Rd <br> Southbound |  |  |  |  | $\begin{array}{\|l\|} \hline 23 \text { rd St } \\ \text { Westbound } \end{array}$ |  |  |  |  |  | $\begin{array}{\|l\|} \hline 1600 \mathrm{Rd} \\ \text { Northbound } \end{array}$ |  |  |  |  |  | $\begin{array}{\|l\|} \hline 23 \text { rd St } \\ \text { Eastbound } \\ \hline \end{array}$ |  |  |  |  |  | Int |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time | R | T | L U | App P | Ped* | R | T | L | U | App | Ped* | R | T | L | U | App | Ped* | R | T | L | U |  | Ped* |  |
| 2:45PM | 3 | 1 | 0 0 | 4 | 0 | 0 | 95 | 4 | 0 | 99 | 0 | 7 | 2 | 15 | 0 | 24 | 1 | 15 | 154 | 9 | 0 | 178 | 1 | 305 |
| Hourly Total | 24 | 6 | 10 | 31 | 0 | 0 | 377 | 18 | 0 | 395 | 0 | 28 | 4 | 50 | 0 | 82 | 1 | 39 | 586 | 25 | 0 | 650 | 1 | 1158 |
| 3:00PM | 11 | 3 | 0 0 | 14 | 0 | 0 | 87 | 5 | 0 | 92 | 0 | 6 | 1 | 12 | 0 | 19 | 0 | 17 | 136 | 5 | 0 | 158 | 0 | 283 |
| 3:15PM | 3 | 1 | 0 | 4 | 0 | 0 | 108 | 6 | 0 | 114 | 0 | 4 | 2 | 12 | 0 | 18 | 0 | 14 | 138 | 9 | 0 | 161 | 0 | 297 |
| 3:30PM | 8 | 13 | 0 0 | 21 | 0 | 1 | 134 | 11 | 0 | 146 | 0 | 9 | 2 | 16 | 0 | 27 | 0 | 21 | 129 | 3 | 0 | 153 | 0 | 347 |
| 3:45PM | 4 | 0 | 0 0 | 4 | 0 | 0 | 110 | 16 | 0 | 126 | 0 | 3 | 3 | 13 | 0 | 19 | 0 | 17 | 157 | 7 | 1 | 182 | 0 | 331 |
| Hourly Total | 26 | 17 | 0 0 | 43 | 0 | 1 | 439 | 38 | 0 | 478 | 0 | 22 | 8 | 53 | 0 | 83 | 0 | 69 | 560 | 24 | 1 | 654 | 0 | 1258 |
| 4:00PM | 14 | 5 | 0 0 | 19 | 0 | 0 | 121 | 15 | 0 | 136 | 0 | 3 | 2 | 15 | 0 | 20 | 0 | 19 | 162 | 8 | 1 | 190 | 0 | 365 |
| 4:15PM | 5 | 0 | 10 | 6 | 0 | 0 | 118 | 17 | 0 | 135 | 0 | 7 | 0 | 10 | 0 | 17 | 0 | 15 | 203 | 5 | 1 | 224 | 0 | 382 |
| 4:30PM | 31 | 8 | 10 | 40 | 0 | 0 | 181 | 21 | 0 | 202 | 0 | 5 | 0 | 16 | 0 | 21 | 0 | 12 | 162 | 1 | 0 | 175 | 0 | 438 |
| 4:45PM | 12 | 2 | 10 | 15 | 0 | 1 | 175 | 13 | 0 | 189 | 0 | 8 | 0 | 12 | 0 | 20 | 0 | 25 | 182 | 3 | 0 | 210 | 0 | 434 |
| Hourly Total | 62 | 15 | 30 | 80 | 0 | 1 | 595 | 66 | 0 | 662 | 0 | 23 | 2 | 53 | 0 | 78 | 0 | 71 | 709 | 17 | 2 | 799 | 0 | 1619 |
| 5:00PM | 9 | 10 | 0 | 20 | 0 | 2 | 157 | 20 | 0 | 179 | 0 | 9 | 2 | 16 | 0 | 27 | 0 | 24 | 182 | 3 | 1 | 210 | 0 | 436 |
| 5:15PM | 9 | 2 | 0 0 | 11 | 0 | 1 | 158 | 17 | 0 | 176 | 0 | 6 | 1 | 11 | 0 | 18 | 0 | 28 | 243 | 2 | 0 | 273 | 0 | 478 |
| 5:30PM | 17 | 2 | 0 0 | 19 | 0 | 0 | 233 | 19 | 0 | 252 | 0 | 8 | 0 | 14 | 0 | 22 | 0 | 17 | 162 | 3 | 0 | 182 | 0 | 475 |
| 5:45PM | 11 | 4 | 0 0 | 15 | 0 | 2 | 194 | 12 | 0 | 208 | 0 | 7 | 0 | 17 | 1 | 25 | 0 | 19 | 137 | 3 | 0 | 159 | 0 | 407 |
| Hourly Total | 46 | 18 | 10 | 65 | 0 | 5 | 742 | 68 | 0 | 815 | 0 | 30 | 3 | 58 | 1 | 92 | 0 | 88 | 724 | 11 | 1 | 824 | 0 | 1796 |
| 6:00PM | 24 | 2 | 0 0 | 26 | 0 | 0 | 188 | 12 | 0 | 200 | 0 | 4 | 1 | 21 | 0 | 26 | 1 | 6 | 141 | 1 | 0 | 148 | 1 | 400 |
| 6:15PM | 12 | 1 | 10 | 14 | 0 | 1 | 186 | 11 | 0 | 198 | 0 | 5 | 0 | 16 | 0 | 21 | 0 | 18 | 114 | 4 | 0 | 136 | 1 | 369 |
| 6:30PM | - 8 | 1 | 0 0 | 9 | 0 | 0 | 192 | 4 | 0 | 196 | 0 | 7 | 2 | 11 | 0 | 20 | 0 | 15 | 111 | 4 | 0 | 130 | 0 | 355 |
| 6:45PM | 5 | 0 | 0 | 5 | 0 | 0 | 181 | 7 | 0 | 188 | 0 | 4 | 1 | 13 | 0 | 18 | 0 | 6 | 110 | 2 | 1 | 119 | 0 | 330 |
| Hourly Total | 49 | 4 | 10 | 54 | 0 | 1 | 747 | 34 | 0 | 782 | 0 | 20 | 4 | 61 | 0 | 85 | 1 | 45 | 476 | 11 | 1 | 533 | 2 | 1454 |
| 7:00PM | 14 | 0 | 0 0 | 14 | 0 | 1 | 185 | 7 | 0 | 193 | 0 | 4 | 0 | 14 | 0 | 18 | 0 | 15 | 67 | 4 | 0 | 86 | 0 | 311 |
| 7:15PM | 6 | 0 | 0 0 | 6 | 0 | 2 | 177 | 6 | 0 | 185 | 0 | 2 | 0 | 4 | 0 | 6 | 0 | 18 | 107 | 4 | 0 | 129 | 0 | 326 |
| 7:30PM | 8 | 4 | 10 | 13 | 0 | 0 | 159 | 5 | 0 | 164 | 0 | 1 | 0 | 6 | 0 | 7 | 0 | 8 | 80 | 2 | 1 | 91 | 0 | 275 |
| 7:45PM | 4 | 0 | 0 | 5 | 0 | 0 | 106 | 4 | 0 | 110 | 0 | 0 | 0 | 7 | 0 | 7 | 0 | 14 | 78 | 3 | 0 | 95 | 0 | 217 |
| Hourly Total | 32 | 4 | 20 | 38 | 0 | 3 | 627 | 22 | 0 | 652 | 0 | 7 | 0 | 31 | 0 | 38 | 0 | 55 | 332 | 13 | 1 | 401 | 0 | 1129 |
| 8:00PM | 14 | 1 | 0 0 | 15 | 0 | 0 | 101 | 4 | 0 | 105 | 0 | 6 | 0 | 5 | 0 | 11 | 0 | 11 | 69 | 1 | 0 | 81 | 2 | 212 |
| 8:15PM | 7 | 0 | 0 0 | 7 | 0 | 0 | 93 | 8 | 0 | 101 | 0 | 3 | 2 | 6 | 0 | 11 | 0 | 14 | 70 | 2 | 0 | 86 | 0 | 205 |
| 8:30PM | 7 | 0 | 0 0 | 7 | 0 | 0 | 85 | 2 | 0 | 87 | 0 | 1 | 0 | 7 | 0 | 8 | 0 | 10 | 74 | 2 | 0 | 86 | 0 | 188 |
| 8:45PM | 2 | 1 | 0 0 | 3 | 0 | 0 | 73 | 6 | 0 | 79 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 8 | 53 | 1 | 2 | 64 | 0 | 147 |
| Hourly Total | 30 | 2 | 0 0 | 32 | 0 | 0 | 352 | 20 | 0 | 372 | 0 | 10 | 2 | 19 | 0 | 31 | 0 | 43 | 266 | 6 | 2 | 317 | 2 | 752 |
| 9:00PM | 2 | 0 | 0 0 | 2 | 0 | 0 | 79 | 6 | 0 | 85 | 0 | 0 | 0 | 5 | 0 | 5 | 0 | 5 | 63 | 1 | 0 | 69 | 0 | 161 |
| 9:15PM | 3 | 0 | 0 0 | 3 | 0 | 0 | 70 | 7 | 0 | 77 | 0 | 1 | 0 | 5 | 0 | 6 | 0 | 3 | 56 | 1 | 0 | 60 | 0 | 146 |
| 9:30PM | 6 | 0 | 0 0 | 6 | 0 | 2 | 81 | 4 | 1 | 88 | 0 | - 2 | 0 | 3 | 0 | 5 | 0 | 5 | 39 | 2 | 1 | 47 | 0 | 146 |
| 9:45PM | 0 | 0 | 0 0 | - | 0 | 0 | 54 | 6 | 0 | 60 | 0 | 1 | 2 | 4 | 0 | 7 | 0 | 4 | 30 | 2 | 0 | 36 | 0 | 103 |
| Hourly Total | 11 | 0 | 0 0 | 11 | 0 | 2 | 284 | 23 | 1 | 310 | 0 | 4 | 2 | 17 | 0 | 23 | 0 | 17 | 188 | 6 | 1 | 212 | 0 | 556 |
| 10:00PM | 2 | 0 | 0 0 | 2 | 0 | 0 | 71 | 3 | 0 | 74 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 4 | 43 | 0 | 1 | 48 | 0 | 125 |
| 10:15PM | 0 | 0 | 0 0 | 0 |  | 1 | 60 | 3 | 0 | 64 | 0 | 0 | 1 | 1 | 0 | 2 |  | - 4 | 24 | 0 | 0 | 28 | 0 | 94 |
| 10:30PM | 3 | 0 | 0 0 | 3 | 0 | 0 | 52 | 0 | 0 | 52 | 0 | 1 | 1 | 1 | 0 | 3 | 0 | 2 | 29 | 0 | 0 | 31 | 0 | 89 |
| 10:45PM | 0 | 0 | 0 0 | 0 | 0 | 0 | 59 | 2 | 0 | 61 | 0 | 1 | 0 | 0 | 0 | 1 | , | 3 | 19 | 0 | 0 | 22 | 0 | 84 |
| Hourly Total | 5 | 0 | 0 0 | 5 |  | 1 | 242 | 8 | 0 | 251 | 0 | 2 | 2 | 3 | 0 | 7 |  | 13 | 115 | 0 | 1 | 129 | 0 | 392 |
| 11:00PM | 0 | 0 | 0 0 | 0 | 0 | 0 | 47 | 1 | 0 | 48 | 0 | 1 | 0 | 1 | 0 | 2 | 0 | - 1 | 19 | 2 | 1 | 23 | 0 | 73 |
| 11:15PM | 0 | 0 | 0 0 | 0 |  | 0 | 39 | 1 | 0 | 40 | 0 | 0 | 1 | 0 | 0 | 1 | , | 1 | 15 | 1 | 0 | 17 | 0 | 58 |
| 11:30PM | 3 | 1 | 0 0 | 4 |  | 0 | 33 | 0 | 0 | 33 | 0 | 0 | 0 | 2 | 0 | 2 |  | - 1 | 23 | 1 | 0 | 25 | 0 | 64 |
| 11:45PM | 0 | 0 | 0 0 | 0 | 0 | 0 | 38 | 1 | 0 | 39 | 0 | 0 | 1 | 2 | 0 | 3 | 0 | 2 | 20 | 1 | 1 | 24 | 0 | 66 |
| Hourly Total | 3 | 1 | $0 \quad 0$ | 4 | 0 | 0 | 157 | 3 | 0 | 160 | 0 | 1 | 2 | 5 | 0 | 8 | 0 | 5 | 77 | 5 | 2 | 89 | 0 | 261 |
| Total | 515 | 112 | $19 \quad 0$ | 646 | 0 | 17 | 8357 | 395 | 3 | 8772 | 0 | 482 | 85 | 825 | 1 | 1393 | 3 | 774 | 8583 | 289 | 18 | 9664 | 6 | 20475 |
| \% Approach | 79.7\% | 17.3\% | 2.9\% 0\% | - |  | 0.2\% 9 | 95.3\% | 4.5\% | 0\% | - |  | 34.6\% | 6.1\% | 59.2\% | 0.1\% | - |  | 8.0\% | 88.8\% | 3.0\% | 0.2\% | - |  |  |
| \% Total | 2.5\% | 0.5\% | 0.1\% 0\% | 3.2\% |  | 0.1\% | 40.8\% | 1.9\% |  | 42.8\% |  | 2.4\% | 0.4\% | 4.0\% | 0\% | 6.8\% |  | 3.8\% | 41.9\% | 1.4\% | 0.1\% | 47.2\% |  |  |
| Lights | 450 | 105 | $17 \quad 0$ | 572 |  | 17 | 8126 | 389 | 3 | 8535 |  | 470 | 84 | 710 | 1 | 1265 |  | 724 | 8293 | 224 | 18 | 9259 |  | 19631 |
| \% Lights | 87.4\% | 93.8\% | 89.5\% 0\% | 88.5\% |  | 100\% 9 | 97.2\% | 98.5\% | 100\% | 97.3\% |  | 97.5\% | 98.8\% | 86.1\% |  | 90.8\% |  | 93.5\% 9 | 96.6\% | 77.5\% | 100\% | 95.8\% |  | 95.9\% |
| Articulated Trucks | 9 | 2 | 10 | 12 |  | 0 | 68 | 2 | 0 | 70 |  | 6 | 0 | 2 | 0 | 8 |  | 3 | 90 | 15 | 0 | 108 |  | 198 |
| \% Articulated Trucks | 1.7\% | 1.8\% | 5.3\% 0\% | 1.9\% |  | 0\% | 0.8\% | 0.5\% | 0\% | 0.8\% |  | 1.2\% | 0\% | 0.2\% | 0\% | 0.6\% |  | 0.4\% | 1.0\% | 5.2\% | 0\% | 1.1\% |  | 1.0\% |
| Buses and Single-Unit Trucks | 56 | 5 | 10 | 62 |  | 0 | 163 | 4 | 0 | 167 |  | 6 | 1 | 113 | 0 | 120 |  | 47 | 200 | 50 | 0 | 297 |  | 646 |
| \% Buses and Single- Unit Trucks | 10.9\% | 4.5\% | 5.3\% 0\% | 9.6\% |  | 0\% | 2.0\% | 1.0\% | 0\% | 1.9\% |  | 1.2\% | 1.2\% | 13.7\% | 0\% | 8.6\% |  | 6.1\% | 2.3\% | 17.3\% | 0\% | 3.1\% |  | 3.2\% |
| Pedestrians | - | - | - - | - |  | - | - | - | - | - | 0 | - | - | - | - | - | 3 | - | - | - | - | - |  |  |
| \% Pedestrians | - | - | - - |  |  | - |  | - |  |  |  | - |  | - | - |  | 100\% | - | - | - | - |  | 83.3\% |  |
| Bicycles on Crosswalk |  |  | - - |  |  | - |  |  |  |  |  | - |  | - - | - | - | 0 | - | - | - | - | - | 1 |  |
| \% Bicycles on Crosswalk | - | - | - - | - |  | - | - | - | - | - |  | - - | - | - | - | - | 0\% | - | - | - | - |  | 16.7\% |  |

*Pedestrians and Bicycles on Crosswalk. L: Left, R: Right, T:Thru, U: U-Turn

Tue Dec 3, 2019
Full Length (12 AM-12 AM (+1))
All Classes (Lights, Articulated Trucks, Buses and Single-Unit Trucks, Pedestrians, Bicycles on Crosswalk)
All Movements
ID: 731785, Location: 38.942698, -95.204907
[N] 1600 Rd
Total: 1037
In: 646 Out: 391


Out: 1282 In: 1393
Total: 2675
[S] 1600 Rd

Tue Dec 3, 2019
AM Peak (Dec 03 2019 7:45AM - 8:45 AM)
All Classes (Lights, Articulated Trucks, Buses and Single-Unit Trucks, Pedestrians, Bicycles on Crosswalk)
'1)
Provided by: Ge walt Hamilton Associates Inc. 625 Forest Edge Drive, Vernon Hills, IL, 60061, US

All Movements
ID: 731785, Location: 38.942698, -95.204907

| Leg <br> Direction | 1600 Rd <br> Southbound |  |  |  |  |  | 23rd St <br> Westbound |  |  |  |  |  |  |  | $\begin{aligned} & 1600 \text { Rd } \\ & \text { Northbound } \end{aligned}$ |  |  |  |  |  | 23rd St <br> Eastbound |  |  |  |  |  | Int |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time | R | T | L | U | App | ed* |  | R | T | L | U |  | App | d* | R | T | L | U | App |  | R | T | L | U | App |  |  |
| 2019-12-03 7:45AM | 6 | 1 |  | 0 | 8 | 0 |  | 0 | 111 | 3 | 0 |  | 114 | 0 | 15 | 8 | 36 | 0 | 59 | 0 | 7 | 173 | 13 | 0 | 193 | 0 | 374 |
| 8:00AM | 16 | 1 | 0 | 0 | 17 | 0 |  | 0 | 112 | 2 | 0 |  | 114 | 0 | 16 | 0 | 24 | 0 | 40 | 0 | 15 | 146 | 1 | 0 | 162 | 0 | 333 |
| 8:15AM | 10 | 0 | 2 | 0 | 12 | 0 |  | 0 | 140 | 2 | 0 |  | 142 | 0 | 11 | 1 | 15 | 0 | 27 | 0 | 13 | 142 | 11 | 0 | 166 | 0 | 347 |
| 8:30 AM | 9 | 1 | 0 | 0 | 10 | 0 |  | 0 | 189 | 1 | 1 |  | 191 | 0 | 12 | 6 | 17 | 0 | 35 | 0 | 10 | 132 | 5 | 0 | 147 | 0 | 383 |
| Total | 41 | 3 | 3 | 0 | 47 | 0 |  | 0 | 552 | 8 | 1 |  | 561 | 0 | 54 | 15 | 92 | 0 | 161 | 0 | 45 | 593 | 30 | 0 | 668 | 0 | 1437 |
| \% Approach | 87.2\% | 6.4\% | 6.4\% 0 |  | - |  |  | \% 9 | 98.4\% | 1.4\% | 0.2\% |  | - |  | 33.5\% | 9.3\% | 57.1\% 0 | \% | - |  | 6.7\% | 88.8\% | 4.5\% 0 |  | - |  |  |
| \% Total | 2.9\% | 0.2\% | 0.2\% 0 | 0\% | 3.3\% |  |  | \% 3 | 38.4\% | 0.6\% | 0.1\% |  | 39.0\% |  | 3.8\% | 1.0\% | 6.4\% 0 | \% | 11.2\% |  | 3.1\% | 41.3\% | 2.1\% 0 | \% | 46.5\% |  |  |
| PHF | 0.641 | 0.750 | 0.375 | - | 0.691 |  |  |  | 0.730 | 0.667 | 0.250 |  | 0.734 |  | 0.8440 | 0.469 | 0.639 | - | 0.682 |  | 0.750 | 0.857 | 0.577 | - | 0.865 |  | 0.938 |
| Lights | 35 | 2 | 23 | 0 | 40 |  |  | 0 | 533 | 7 | 1 |  | 541 |  | 53 | 15 | 75 | 0 | 143 |  | 36 | 579 | 27 | 0 | 642 |  | 1366 |
| \% Lights | 85.4\% | 66.7\% | 100\% 0 | 0\% | 85.1\% |  |  | \% 9 | 96.6\% | 87.5\% | 100\% |  | 9.4 \% |  | 98.1\% | 100\% | 81.5\% 0 | \% | 88.8\% |  | 80.0\% | 97.6\% | 90.0\% 0 |  | 96.1\% |  | 95.1\% |
| Articulated Trucks | 0 | 0 | 0 | 0 | 0 |  |  | 0 | 4 | 0 | 0 |  | 4 |  | 0 | 0 | 0 | 0 | 0 |  | 0 | 5 | 0 | 0 | 5 |  | 9 |
| \% Articulated Trucks | 0\% | 0\% | 0\% 0 |  | 0 \% |  | -0\% |  | 0.7\% | 0\% | 0\% |  | 0.7\% |  | 0\% | 0\% | 0\% 0\% | \% | 0\% |  | 0\% | 0.8\% | 0\% 0 |  | 0.7\% |  | 0.6\% |
| Buses and Single-Unit Trucks | 6 | 1 | 10 | 0 | 7 |  |  |  | 15 | 1 | 0 |  | 16 |  | 1 | 0 | 17 | 0 | 18 |  | 9 | 9 | 3 | 0 | 21 |  | 62 |
| \% Buses and Single Unit Trucks | 14.6\% | 33.3\% | 0\% 0 |  | 14.9\% |  | - 0\% |  | 2.7\% | 12.5\% | 0\% |  | 2.9\% |  | 1.9\% | 0\% | 18.5\% 0 | \% | 11.2\% |  | 20.0\% | 1.5\% | 10.0\% 0 |  | 3.1\% |  | 4.3\% |
| Pedestrians | - |  | - - | - | - | 0 |  | - | - | - | - - |  | - | 0 | - | - | - |  | - | 0 | - | - | - | - | - | 0 |  |
| \% Pedestrians | - |  | - - | - | - |  |  | - | - | - | - - |  | - |  | - | - | - | - | - |  | - | - | - | - | - |  |  |
| Bicycles on Crosswalk | - |  | - - |  |  | 0 |  | - | - | - |  |  | - | 0 | - | - | - | - | - | 0 | - | - | - | - | - | 0 |  |
| \% Bicycles on Crosswalk | - |  | - |  | - |  |  | - |  | - |  |  | - |  | - | - | - | - | - |  | - | - | - | - | - |  |  |

[^0]AM Peak (Dec 03 2019 7:45AM - 8:45 AM)
All Classes (Lights, Articulated Trucks, Buses and Single-Unit Trucks, Pedestrians, Bicycles on Crosswalk)
All Movements
ID: 731785, Location: 38.942698, -95.204907
[N] 1600 Rd
Total: 92
In: $47 \quad$ Out: 45


Out: $56 \quad \ln : 161$
Total: 217
[S] 1600 Rd

E 23rd Street \& E 1600 Road - TMC
Tue Dec 3, 2019
Midday Peak (Dec 032019 12PM - 1 PM)
All Classes (Lights, Articulated Trucks, Buses and Single-Unit Trucks, Pedestrians, Bicycles on Crosswalk)

Provided by: Gewalt Hamilton Associates Inc. 625 Forest Edge Drive, Vernon Hills, IL, 60061, US

ID: 731785, Location: 38.942698, -95.204907

| Leg <br> Direction | 1600 Rd Southbound |  |  |  |  |  | 23rd St <br> Westbound |  |  |  |  |  | $\begin{aligned} & 1600 \mathrm{Rd} \\ & \text { Northbound } \end{aligned}$ |  |  |  |  |  | $\begin{array}{\|l\|} \hline 23 \text { rd St } \\ \text { Eastbound } \end{array}$ |  |  |  |  |  | Int |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time | R | T | L | U | App |  | R | T | L | U | App |  | R | T |  | U | App |  | R | T | L | U | App | Ped* |  |
| 2019-12-03 12:00PM | 9 | 6 | 0 | 0 | 15 | 0 | 0 | 97 | 4 | 0 | 101 | 0 | 6 | 0 | 18 | 0 | 24 | 0 | 14 | 122 | 2 | 0 | 138 | 0 | 278 |
| 12:15PM | 6 | 3 | 0 | 0 | 9 | 0 | 0 | 104 | 2 | 0 | 106 | 0 | 6 | 0 | 10 | 0 | 16 | 0 | 10 | 130 | 5 | 1 | 146 | 0 | 277 |
| 12:30PM | 8 | 3 | 1 | 0 | 12 | 0 | 1 | 112 | 2 | 0 | 115 | 0 | 4 | 2 | 12 | 0 | 18 | 0 | 18 | 123 | 3 | 0 | 144 | 0 | 289 |
| 12:45PM | 14 | 2 | 0 |  | 16 | 0 | 0 | 114 | 5 | 0 | 119 | 0 | 4 | 0 | 15 | 0 | 19 | 0 | 12 | 112 | 8 | 0 | 132 | 0 | 286 |
| Total | 37 | 14 | 1 | 0 | 52 | 0 | 1 | 427 | 13 | 0 | 441 | 0 | 20 | 2 | 55 | 0 | 77 | 0 | 54 | 487 | 18 | 1 | 560 | 0 | 1130 |
| \% Approach | 71.2\% | 26.9\% | 1.9\% |  | - | - | 0.2\% | 96.8\% | 2.9\% |  | - |  | 26.0\% | 2.6\% | 71.4\% | 0\% | - | - | 9.6\% | 87.0\% | 3.2\% | 0.2\% | - |  |  |
| \% Total | 3.3\% | 1.2\% | 0.1\% | 0\% | 4.6 \% | - | 0.1\% | 37.8\% | 1.2\% |  | 39.0\% |  | 1.8\% | 0.2\% | 4.9\% | 0\% | 6.8 \% |  | 4.8\% | 43.1\% | 1.6\% | 0.1\% | 49.6 \% | - |  |
| PHF | 0.661 | 0.583 | 0.250 | - | 0.813 | - | 0.250 | 0.936 | 0.650 |  | 0.926 |  | 0.833 | 0.250 | 0.764 | - | 0.802 |  | 0.750 | 0.937 | 0.563 | 0.250 | 0.959 |  | 0.978 |
| Lights | 32 | 12 | 1 | 0 | 45 | - | 1 | 400 | 13 | 0 | 414 | - | 19 | 2 | 45 | 0 | 66 |  | 52 | 462 | 14 | 1 | 529 |  | 1054 |
| \% Lights | 86.5\% | 85.7\% | 100\% | 0\% | 86.5\% | - | 100\% | 93.7\% | 100\% |  | 93.9\% |  | 95.0\% | 100\% | 81.8\% | 0\% | 85.7\% |  | 96.3\% | 94.9\% | 77.8\% | 100\% | 94.5\% |  | 93.3\% |
| Articulated Trucks | 0 | 1 | 0 | 0 | 1 | - | 0 | 6 | 0 | 0 | 6 | - | 0 | 0 | 1 | 0 | 1 | - | 0 | 7 | 0 | 0 | 7 | - | 15 |
| \% Articulated Trucks | 0\% | 7.1\% | 0\% | 0\% | 1.9\% | - | 0\% | 1.4\% | 0\% |  | 1.4 \% |  | 0\% | 0\% | 1.8\% |  | 1.3 \% | - | 0\% | 1.4\% | 0\% | 0\% | 1.3 \% | - | 1.3\% |
| Buses and Single-Unit Trucks | 5 | 1 | 0 | 0 | 6 | - | 0 | 21 | 0 | 0 | 21 | - | 1 | 0 | 9 | 0 | 10 | - | 2 | 18 | 4 | 0 | 24 | - | 61 |
| \% Buses and SingleUnit Trucks | 13.5\% | 7.1\% | 0\% | 0\% | 11.5\% | - | 0\% | 4.9\% | 0\% |  | 4.8 \% | - | 5.0\% | 0\% | 16.4\% | 0\% | 13.0\% | - | 3.7\% | 3.7\% | 22.2\% | 0\% | 4.3 \% | - | 5.4\% |
| Pedestrians | - | - | - | - | - | 0 | - | - | - - | - | - | 0 | - | - |  | - - | - | 0 | - | - | - | - | - | 0 |  |
| \% Pedestrians | - | - | - | - | - | - | - | - | - - | - | - | - | - | - |  | - | - | - | - | - | - | - | - | - | - |
| Bicycles on Crosswalk | - | - | - | - | - | 0 | - | - | - - | - | - | 0 | - | - |  | - | - | 0 | - | - | - | - | - | 0 |  |
| \% Bicycles on Crosswalk | - | - | - | - | - |  | - | - | - - |  | - | - | - | - |  | - | - |  | - | - | - | - | - | - | - |

*Pedestrians and Bicycles on Crosswalk. L: Left, R: Right, T: Thru, U: U-Turn

Tue Dec 3, 2019
Midday Peak (Dec 032019 12PM - 1 PM)
All Classes (Lights, Articulated Trucks, Buses and Single-Unit Trucks, Pedestrians, Bicycles on Crosswalk)
All Movements
ID: 731785, Location: 38.942698, -95.204907
[N] 1600 Rd
Total: 73
In: $52 \quad$ Out: 21


Out: $81 \quad \ln : 77$
Total: 158
[S] 1600 Rd

Tue Dec 3, 2019
PM Peak (Dec 032019 4:45PM - 5:45 PM) - Overall Peak Hour
All Classes (Lights, Articulated Trucks, Buses and Single-Unit Trucks, Pedestrians, Bicycles on Crosswalk)

CHIMAGEWAL HAMILON
Provided by: Gewalt Hamilton Associates Inc. 625 Forest Edge Drive, Vernon Hills, IL, 60061, US

ID: 731785, Location: 38.942698, -95.204907

| Leg <br> Direction | 1600 Rd <br> Southbound |  |  |  |  |  | 23rd St <br> Westbound |  |  |  |  |  | $\begin{aligned} & 1600 \text { Rd } \\ & \text { Northbound } \end{aligned}$ |  |  |  |  |  | 23rd St <br> Eastbound |  |  |  |  |  | Int |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time | R | T | L | U | App |  | R | R T | L | U | App |  | R | T |  | U | App |  | R | T | L | U | App | Ped* |  |
| 2019-12-03 4:45PM | 12 | 2 | 1 | 0 | 15 | 0 | 1 | 175 | 13 | 0 | 189 | 0 | 8 | 0 | 12 | 0 | 20 | 0 | 25 | 182 | 3 | 0 | 210 | 0 | 434 |
| 5:00PM | 9 | 10 | 1 | 0 | 20 | 0 | 2 | 157 | 20 | 0 | 179 | 0 | 9 | 2 | 16 | 0 | 27 | 0 | 24 | 182 | 3 | 1 | 210 | 0 | 436 |
| 5:15PM | 9 | 2 | 0 | 0 | 11 | 0 | 1 | 158 | 17 | 0 | 176 | 0 | 6 | 1 | 11 | 0 | 18 | 0 | 28 | 243 | 2 | 0 | 273 | 0 | 478 |
| 5:30PM | 17 | 2 | 0 | 0 | 19 | 0 | 0 | 233 | 19 | 0 | 252 | 0 | 8 | 0 | 14 | 0 | 22 | 0 | 17 | 162 | 3 | 0 | 182 | 0 | 475 |
| Total | 47 | 16 | 2 | 0 | 65 | 0 | 4 | 723 | 69 | 0 | 796 | 0 | 31 | 3 | 53 | 0 | 87 | 0 | 94 | 769 | 11 | 1 | 875 | 0 | 1823 |
| \% Approach | 72.3\% | 24.6\% | 3.1\% |  | - | - | 0.5\% | 90.8\% | 8.7\% |  | - |  | 35.6\% | 3.4\% | 60.9\% |  | - |  | 10.7\% | 87.9\% | 1.3\% | 0.1\% | - |  | - |
| \% Total | 2.6\% | 0.9\% | 0.1\% |  | 3.6 \% | - | 0.2\% | 39.7\% | 3.8\% |  | 43.7 \% |  | 1.7\% | 0.2\% | 2.9\% |  | 4.8 \% |  | 5.2\% | 42.2\% | 0.6\% | 0.1\% | 48.0 \% | - | - |
| PHF | 0.691 | 0.400 | 0.500 | - | 0.813 | - | 0.500 | 0.776 | 0.863 | - | 0.790 |  | 0.861 | 0.375 | 0.828 |  | 0.806 |  | 0.839 | 0.791 | 0.917 | 0.250 | 0.801 |  | 0.953 |
| Lights | 43 | 16 | 2 | 0 | 61 | - | 4 | 709 | 69 | 0 | 782 |  | 29 | 2 | 49 | 0 | 80 |  | 93 | 758 | 6 | 1 | 858 |  | 1781 |
| \% Lights | 91.5\% | 100\% | 100\% | 0\% | 93.8\% | - | 100\% | 98.1\% | 100\% | 0\% | 98.2\% |  | 93.5\% | 66.7\% | 92.5\% |  | 92.0\% |  | 98.9\% | 98.6\% | 54.5\% | 100\% | 98.1\% |  | 97.7\% |
| Articulated Trucks | 2 | 0 | 0 | 0 | 2 | - | 0 | 4 | 0 | 0 | 4 |  | 1 | 0 | 0 | 0 | 1 |  | 1 | 3 | 2 | 0 | 6 | - | 13 |
| \% Articulated Trucks | 4.3\% | 0\% | 0\% |  | 3.1\% | - | 0\% | 0.6\% | 0\% |  | 0.5 \% |  | 3.2\% | 0\% | 0\% |  | 1.1\% |  | 1.1\% | 0.4\% | 18.2\% | 0\% | 0.7 \% |  | 0.7\% |
| Buses and Single-Unit Trucks | 2 | 0 | 0 | 0 | 2 | - | 0 | 10 | 0 | 0 | 10 | - | 1 | 1 | 4 | 0 | 6 | - | 0 | 8 | 3 | 0 | 11 | - | 29 |
| \% Buses and SingleUnit Trucks | 4.3\% | 0\% | 0\% |  | 3.1\% | - | 0\% | 1.4\% |  |  | 1.3\% | - | 3.2\% | 33.3\% | 7.5\% |  | 6.9 \% | - | 0\% | 1.0\% | 27.3\% | 0\% | 1.3 \% | - | 1.6\% |
| Pedestrians | - | - | - | - | - | 0 | - | - | - - | - | - | 0 | - | - | - | - | - | 0 | - | - | - | - - | - - | 0 |  |
| \% Pedestrians | - | - | - | - | - | - | - | - | - - | - | - |  | - - | - | - | - | - |  | - | - |  | - - | - - | - | - |
| Bicycles on Crosswalk | - | - | - | - | - | 0 | - | - - | - - | - | - | 0 | - | - | - | - - | - | 0 | - | - |  | - - | - - | 0 |  |
| \% Bicycles on Crosswalk | - | - | - | - | - | - | - | - - | - - | - | - | - | - - | - | - | - | - | - | - - | - |  | - - | - - | - | - |

*Pedestrians and Bicycles on Crosswalk. L: Left, R: Right, T: Thru, U: U-Turn

Tue Dec 3, 2019
PM Peak (Dec 032019 4:45PM - 5:45 PM) - Overall Peak Hour
All Classes (Lights, Articulated Trucks, Buses and Single-Unit Trucks, Pedestrians, Bicycles on Crosswalk)
All Movements
ID: 731785, Location: 38.942698, -95.204907
[ N$] 1600 \mathrm{Rd}$
Total: 83
In: 65 Out: 18


Out: $179 \quad \ln : 87$
Total: 266
[S] 1600 Rd

|  |  |  |  |  |  |  |  | Fixe |  | F_of_ | Tota | Fatal_ | Injur | O- | F_of_ | of |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Accident_K | Date | On_Road | Dist | UOM | Dir | Accident_C | cwov | Obje | Accident_L | Vehs | Accs | Accs | Acc | Accs | Deat | Inju | Time | Weather_Co | Light_Cond | KDOT_Latit | KDOT_Longi |
| 20140101562 | 1/27/2014 | K010 | 1 | F | N | COLL W FIXED OBJECT |  |  | INTRSECTION-RELATED-ON ROADWAY | 1 | 1 | 0 | 0 | 1 | 0 | 0 | 1203 | NO ADVERSE CONDITIONS | DAYLIGHT | 38.94266 | -95.20481 |
| 20140107615 | 4/17/2014 | к010 | 0 |  |  | COLL W Other motor vehicle | ANGLE - SIDE IMPACT |  | Intersection-on roadway | 2 | 1 | 0 | 1 | 0 | 0 | 3 | 2256 | No AdVERSE CONDITIONS | dark--street lights on | 38.94266 | -95.20481 |
| 20140108155 | 5/2/2014 | к010 | 0 |  |  | COLL W Other motor vehicle | rear end |  | intersection-on roadway | 2 | 1 | 0 | 0 | 1 | 0 | 0 | 2240 | No AdVERSE CONDITİNS | dark--street lights on | 38.94266 | -95.20481 |
| 20140108161 | 4/30/2014 | к010 | 20 | F | w | coll w other motor vehicle | SIDESWIPE: SAME DIRECTION |  | intrsection-related-on roadway | 3 | 1 | 0 | 0 | 1 | 0 | 0 | 1605 | no adverse conditions | DAYLIGHT | 38.94266 | -95.20489 |
| 20140108248 | 5/2/2014 | к010 | 30 | F | E | coll w other motor vehicle | rear end |  | intrsection-related-on roadway | 2 | 1 | 0 | 1 | 0 | 0 | 1 | 2230 | No ADVERSE CONDITIONS | dark--street lights on | 38.94266 | -95.2047 |
| 20140109535 | 5/13/2014 | к010 | 0 |  |  | COLL $W$ Other motor vehicle | rear end |  | Intersection-On roadway | 2 | 1 | 0 | 1 | 0 | 0 | 1 | 1405 | NO ADVERSE CONDITIONS | DAYLIGHT | 38.9426 | -95.20481 |
| 20140111174 | 6/11/2014 | к010 | 300 | F | w | COLL W Other motor vehicle | rear end |  | Intreection-related-on roadway | 2 | 1 | 0 | 0 | 1 | 0 | 0 | 1805 | NO ADVERSE CONDITIONS | DAYLIGHT | 38.94267 | -95.20587 |
| 20140111696 | 6/18/2014 | ко | 100 | F | w | coll w other motor vehicle | rear end |  | NON-INTERSECTION-ON ROADWAY | 2 | 1 | 0 | 0 | 1 | 0 | 0 | 843 | No ADVERSE CONDITIONS | DAYLIGHT | 38.9426 | -95.20516 |
| 20140113218 | 7/10/2014 | 10 | 50 | F | w | coll w other motor vehicle | rear end |  | Intrsection-related-on roadway | 2 | 1 | 0 | 0 | 1 | 0 | 0 | 1819 | no adverse conditions | DAYLIGHT | 38.9426 | -95.20498 |
| 20140116797 | 8/23/2014 | к010 | 20 | F | w | coll w other motor vehicle | rear end |  | intrsection-related-on roadway | 2 | 1 | 0 | 1 | 0 | 0 | 1 | 1210 | no adverse conditions | daylight | 38.94266 | -95.20496 |
| 20140124649 | 11/14/2014 | к010 | 0.1 | M | w | coll w other motor vehicle | rear end |  | NON-INTERSECTION-ON ROADWAY | 2 | 1 | 0 | 1 | 0 | 0 | 1 | 1555 | no AdVERSE CONDITİNS | DAYLIGHT | 38.94267 | -95.20674 |
| 20140124894 | 11/17/2014 | к010 | 10 | F | E | COLL $W$ Other motor vehicle | Rear end |  | Intrsection-related-on roadway | 3 | 1 | 0 | 0 | 1 | 0 | 0 | 1920 | NO ADVERSE CONDITIONS | DARK--NO STREET LIGHTS | 38.94266 | -95.20485 |
| 20140125445 | 11/22/2014 | к010 | 600 | F | w | coll w other motor vehicle | rear end |  | intrsection-related-on roadway | 3 | 1 | 0 | 0 | 1 | 0 | 0 | 1510 | no adverse conditions | daylight | 38.94268 | -95.207 |
| 20140128003 | 12/16/2014 | к010 | 10 | F | w | coll w other motor vehicle | rear end |  | intrsection-related-on roadway | 2 | 1 | 0 | 0 | 1 | 0 | 0 | 1520 | no adverse Conditions | DAYLIGHT | 38.94266 | -95.20492 |



|  |  |  |  |  |  |  |  |  |  | F_of | Total | Fatal | Injury | PDO- | F_of | F_of_ |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Accident_K | Date | On_Road | Dist | vom | Dir | Accident_C | cwov | Fixed_Obje | Accident_L | Vehs | Accs | Accs | Acc | Accs | Deat | Inju | Time | Weather_Co |  | Light_Cond | KDOT_Latit | KDOT_Longi |
| 20160033260 | 1/6/2016 | к010 | 50 | F | E | COLL w Other motor vehicle | rear end |  | intrsection-relatedoon roadway | 3 | 1 | 0 | 0 | 1 | 0 | 0 | 1640 | NO ADVERSE CONDITIONS |  | daylight | 38.94266 | -95.20472 |
| 20160101811 | 1/30/2016 | к010 | 1 | F | w | coll w fixed object |  | CURB | ROADSIDE-NO SHLDR-OfF RDWY | 1 | 1 | 0 | 0 | 1 | 0 | 0 | 1248 | NO ADVERSE CONDITIONS |  | DAYLIGHT | 38.94266 | -95.2049 |
| 20160102739 | 2/13/2016 | к010 | 5 | F | w | coll w Fixed object |  | Other post-pole | ROADSIDE-NO SHLDR-OFF RDWY | 1 | 1 | 0 | 0 | 1 | 0 | 0 |  | no AdVERSE CONDITIONS | dark--s | Street lights on | 38.94266 | -95.2049 |
| 20160102820 | 2/11/2016 | k01 | 500 | F | E | COLL w Other motor vehicle | AR End |  | NON-INTERSECTION-ON ROADWAY | 3 | 1 | 0 | 1 | 0 | 0 | 1 | 800 | NO ADVERSE CONDITIONS |  | DAYLIGHT | 38.9426 | -95.20312 |
| 20160103755 | 2/27/2016 | к010 | 300 | F | w | coll w other motor vehicle | rear end |  | intrsection-relatedoon roadway | 2 | 1 | 0 | 0 | 1 | 0 | 0 | 1304 | no ADVERSE CONDITİNS |  | DAYLIGHT | 38.9426 | -95.20594 |
| 20160104193 | 3/3/2016 | к010 | 0 |  |  | COLL W OTHER MOTOR VEHICLE | ANGLE - SIDE IMPACT |  | intersection-on roadway | 2 | 1 | 0 | 0 | 1 | 0 | 0 | 1115 | no Adverse conditions |  | DAYLIGHT | 38.94266 | -95.20488 |
| 20160104206 | 2/26/2016 | к010 | 286 | F | w | coll w other motor vehicle | rear end |  | intrsection-related-on roadway | 2 | 1 | 0 | 0 | 1 | 0 | 0 | 1701 | NO ADVERSE CONDITIIONS |  | DAYLIGHT | 38.94267 | -95.20589 |
| 20160104706 | 3/3/2016 | к010 | 20 | F | E | coll w other motor vehicle | rear end |  | intrsection-related-on roadway | 2 | 1 | 0 | 0 | 1 | 0 | 0 | 755 | no Adverse Conditions |  | daylight | 38.94266 | -95.20481 |
| 20160107779 | 4/10/2016 | к010 | 200 | F | E | COLL W Animal |  |  | NON-INTERSECTION-ON ROADWAY | 1 | 1 | 0 | 0 | 1 | 0 | 0 | 38 | NO ADVERSE CONDITIONS | DARK--s | STREET LIGHTS ON | 38.94265 | -95.20418 |
| 20160108048 | 4/10/2016 | к010 | 100 | F | w | coll w other motor vehicle | rear end |  | NON-INTERSECTION-ON ROADWAY | 3 | 1 | 0 | 0 | 1 | 0 | 0 | 1018 | no adverse conditions |  | daylight | 38.94266 | -95.20524 |
| 20160108541 | 4/18/2016 | к010 | 35 | F | w | COLL w Other motor vehicle | rear end |  | intrsection-relatedoon roadway | 2 | 1 | 0 | 0 | 1 | 0 | 0 | 720 | Rain, mist or drizzle |  | DAYLIGHT | 38.94266 | -95.20488 |
| 20160109186 | 4/29/2016 | к010 | 25 | F | E | COLL w Other motor vehicle | rear end |  | intrsection-relatedoon roadway | 2 | 1 | 0 | 1 | 0 |  | 1 | 1609 | Rain, mist or drizzle |  | DAYLIGHT | 38.94266 | -95.20479 |
| 20160110216 | 5/13/2016 | к010 | 300 | F | w | COLL W OTHER MOTOR VEHICLE | rear end |  | Intreection-related-on roadway | 2 | 1 | 0 | 0 | 1 | 0 | 0 | 1722 | RAIN, MIST OR DRIZZLE |  | DAYLIGHT | 38.94267 | -95.20594 |
| 20160110217 | 5/13/2016 | к010 | 16 | F | w | coll w other motor vehicle | rear end |  | intrsection-relatedoon roadway | 2 | 1 | 0 | 0 | 1 | 0 | 0 | 1712 | Rain, mist or drizzle |  | daylight | 38.94266 | -95.20494 |
| 20160111386 | 5/16/2016 | к010 | 12 | F | w | coll w other motor vehicle | rear end |  | intrsection-relatedoon roadway | 2 | 1 | 0 | 0 | 1 | 0 | 0 | 1243 | RAIN, MIST OR DRIZZLE |  | daylight | 38.94266 | -95.20492 |
| 20160112225 | 6/3/2016 | к010 | 15 | F | E | COLL W OTHER MOTOR VEHICLE | Rear end |  | Intrsection-related-on roadway | 2 | 1 | 0 | 1 | 0 | 0 | 2 | 1955 | NO ADVERSE CONDITIONS |  | DAYLIGHT | 38.94266 | -95.20483 |
| 20160113092 | 6/14/2016 | 010 | 500 | F | w | COLL w Other motor vehicle | rear end |  | intrsection-relatedoon roadway | 2 | 1 | 0 | 0 | 1 | 0 | 0 | 700 | no ADVERSE CONDITIONS |  | DAYLIGHT | 38.94267 | -95.20665 |
| 20160113289 | 6/18/2016 | к010 | 0 |  |  | COLL w Other motor vehicle | rear end |  | intersection-on roadway | 2 | 1 | 0 | 0 | 1 | 0 | 0 | 600 | no Adverse conditions |  | DAYLIGHT | 38.94266 | -95.20488 |
| 20160114790 | 6/29/2016 | к010 | 300 | F | w | COLL w Other motor vehicle | rear end |  | intrsection-related-on roadway | 3 | 1 | 0 | 0 | 1 | 0 | 0 | 1555 | NO ADVERSE CONDITIONS |  | DAYLIGHT | 38.94267 | -95.20594 |
| 20160117241 | 7/30/2016 | к010 | 285 | F | E | coll w other motor vehicle | rear end |  | intrsection-relatedoon roadway | 3 | 1 | 0 | 0 | 1 |  | 0 | 1630 | NO ADVERSE CONDITIONS |  | daylight | 38.94265 | -95.20388 |
| 20160117273 | 8/2/2016 | к010 | 20 | F | E | coll w other motor vehicle | rear end |  | intrsection-relatedoon roadway | 2 | 1 | 0 | 0 | 1 | 0 | 0 | 645 | NO ADVERSE CONDITİNS |  | DAYLIGHT | 38.94266 | -95.20481 |
| 20160117529 | 7/15/2016 | к010 | 15 | F | E | COLL w Other motor vehicle | IDESWIPE: SAME DIRECTION |  | NON-Intersection-on roadway | 3 | 1 | 0 | 1 | 0 | 0 | 2 | 2213 | NO ADVERSE CONDITIONS | Dark--s | Street lights on | 38.94266 | -95.20483 |
| 20160118807 | 8/16/2016 | k010 | 45 | F | E | COLL W OTHER MOTOR VEHICLE | REAR END |  | INTRSECTION-RELATED-ON ROADWAY | 3 | 1 | 0 | 0 | 1 | 0 | 0 | 1700 | NO ADVERSE CONDITIONS |  | DAYLIGHT | 38.94266 | -95.20472 |
| 20160119237 | 8/22/2016 | к010 | 100 | F | w | COLL w Other motor vehicle | ANGLE - SIDE IMPACT |  | intrsection-relatedoon roadway | 2 | 1 | 0 | 0 | 1 | 0 | 0 | 719 | no Adverse conditions |  | daylight | 38.94266 | -95.20524 |
| 20160120083 | 9/4/2016 | к010 | 426 | F | E | COLL w Other motor vehicle | rear end |  | intrsection-relatedoon roadway | 3 | 1 | 0 | 0 | 1 | 0 | 0 | 1515 | no Adverse conditions |  | daylight | 38.94264 | -95.20338 |
| 20160120600 | 9/12/2016 | к010 | 0.01 | M | w | COLL W OTHER MOTOR VEHICLE | rear end |  | Intreection-related-on roadway | 2 |  | 0 | 0 | 1 | 0 | 0 | 1618 | NO ADVERSE CONDITIONS |  | DAYLIGHT | 38.94266 | -95.20507 |
| 20160120609 | 9/12/2016 | к010 | 0.1 | M | E | coll w other motor vehicle | rear end |  | intrsection-related-on roadway | 3 | 1 | 0 | 1 | 0 |  | 1 | 1530 | NO ADVERSE CONDITIINS |  | daylight | 38.94264 | -95.20303 |
| 20160122979 | 10/7/2016 | к010 | 350 | F | w | COLL w Other motor vehicle | rear end |  | NON-Intersection-on roadway | 2 | 1 | 0 | 0 | 1 | 0 | 0 | 1640 | NO ADVERSE CONDITIONS |  | DAYLIGHT | 38.94267 | -95.20611 |
| 20160124464 | 10/21/2016 | к010 | 30 | F | w | coll w other motor vehicle | rear end |  | Intrsection-related-on roadway | 2 | 1 | 0 | 1 | 0 | 0 | 1 | 643 | NO ADVERSE CONDITIONS |  | dawn | 38.94266 | -95.20499 |
| 20160124977 | 10/27/2016 | k010 | 25 | F | E | COLL W OTHER MOTOR VEHICLE | REAR END |  | IntRSECTION-RELATED-ON ROADWAY | 2 | 1 | 0 | 1 | 0 | 0 | 1 | 1549 | NO ADVERSE CONDITIONS |  | DAYLIGHT | 38.94266 | -95.20479 |
| 20160125521 | 10/25/2016 | к010 | 220 | F | w | COLL w Other motor vehicle | rear end |  | non-Intersection-on roadway | 2 | 1 | 0 | 1 | 0 |  | 2 | 1636 | no Adverse conditions |  | DAYLIGHT | 38.94266 | -95.20566 |
| 20160126611 | 11/3/2016 | к010 | 35 | F | w | coll w other motor vehicle | rear end |  | Intrsection-related-on roadway | 2 | 1 | 0 | 0 | 1 |  | 0 | 1520 | NO ADVERSE CONDITIONS |  | DAYLIGHT | 38.94266 | -95.20501 |
| 20160101774 | 2/2/2016 | 23RD | 150 | F | w | coll w other motor vehicle | rear end |  | intrsection-relatedoon roadway | 2 | 1 | 0 | 1 | 0 | 0 | 1 | 1733 | no Adverse Conditions |  | dusk | 0 | 0 |
| 20160131860 | 12/17/2016 | 23RD | 15 | F | w | coll w other motor vehicle | rear end |  | NON-INTERSECTION-ON ROADWAY | 2 | 1 | 0 | 0 | 1 | 0 | 0 | 640 | NO ADVERSE CONDITIIONS | dark--s | -Street lights on | 0 | 0 |

Accident_K Date
20170100115 1/3/2017
20170100620 1/12/2017 20170004381 3/2/2017 20170104931 3/10/2017 2170109106 4/27/2017 20170111523 5/15/2017 20170113397 6/13/2017 20170113446 6/16/2017 $201701169838 / 10 / 2017$ 0170120486 9/27/2017 20170120486 9/27/2017 $2017012659711 / 4 / 2017$ 20170126617 10/27/2017 0170127098 11/5/2017 V 20170128611 11/21/2017
 21018065 8/25/2017 VENTURE PARK 20170127098 11/5/2017 VENTUEPARK

|  |  |
| :---: | :---: |
| On_Road | Dist |
| 23RD | 145 |
| 23RD | 158 |
| 23RD | 0.1 |
| 23RD | 100 |
| 23RD | 40 |
| 23RD | 100 |
| 23RD | 300 |
| 23RD | 50 |
| 23RD | 150 |
| 23RD | 200 |
| 23RD | 300 |
| 23RD | 30 |
| 23RD | 30 |
| 23RD | 0 |
| NTUREPARK | 0.5 |
| 23RD | 200 |
| NTURE PARK | 0 |



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COLL W OTHER MOTOR VEHILLE COLL W OTHER MOTOR VEHICLE COLL W FIXED OBJECT W OTHER MOTOR VEHI COLL W OTHER MOTOR VEHICL COLL W PEDESTRIAN COLL W OTHER MOTOR VEHICL COLL W FIXED OBJECT
coll w pedestrian
cwov
rear end
REAR END Rear end REAR END rear end

## - SIDE IMP

## REAR END

REAR END

Accident_L
NON-INTERSECTON-ON ROADWAY NON-INTERSECTION-ON ROADWAY
INTRSECTION-RELATED-ON ROADWA NON-INTERSECTION-ON ROADWAY NON-INTERSECTION-ON ROADWAY intrsection-related-on roadway intriection-related-on roadway NON-INTERSECTION-ON ROADWAY NON-INTERSECTION-ON ROADWAY NON-INTERSECTION-ON ROADWAY NTRSECIONESECTIOD-ON ROADWAY NON-INTERSECTION-ON ROADWAY NON-INTERSECTION-ON ROADWAY INTERSECTION-ON ROADWAY non-Intersection-on roadway NON-INTERSECTION-ON ROADWAY intersection-on roadway NON-INTERSECTION-ON ROADWAY

| of_ | al_ | Fatal_ | Injury_ | PDO_ | F_of_ |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Vehs | Accs | Accs | Acc | Accs | Deat | Inju | Time | Weather_Co | Light_Cond | KDOT_Latit | KDOT_Long |
| 2 | 1 | 0 | 0 | 1 | 0 | 0 | 2307 | NO ADVERSE CONDITIONS | dark--street lights on | 0 | 0 |
| 2 | 1 | 0 | 0 | 1 | 0 | 0 | 1555 | NO ADVERSE Conditions | DAYLIGHT | 0 | 0 |
| 2 | 1 | 0 | 0 | 1 | 0 | 0 | 1731 | NO ADVERSE CONDITIONS | DAYLIGHT | 0 | 0 |
| 3 | 1 | 0 | 0 | 1 | 0 | 0 | 1710 | NO ADVERSE CONDITIONS | DAYLIGHT | 0 | 0 |
| 2 | 1 | 0 | 0 | 1 | 0 | 0 | 1630 | NO ADVERSE CONDITIONS | DAYLIGHT | 0 | 0 |
| 2 | 1 | 0 | 0 | 1 | 0 | 0 | 1545 | NO ADVERSE CONDITIONS | DAYLIGHT | 0 | 0 |
| 1 | 1 | 0 | 1 | 0 | 0 | 1 | 1915 | NO ADVERSE Conditions | DAYLIGHT | 0 | 0 |
| 2 | 1 | 0 | 0 | 1 | 0 | 0 | 1744 | NO ADVERSE CONDITIONS | DAYLIGHT | 0 | 0 |
| 2 | 1 | 0 | 0 | 1 | 0 | 0 | 736 | FOG | DAYLIGHT | 0 | 0 |
| 2 | 1 | 0 | 1 | 0 | 0 | 1 | 1141 | RAIN, MIST OR DRIZZLE | DAYLIGHT | 0 | 0 |
| 2 | 1 | 0 | 0 | 1 | 0 | 0 | 744 | NO ADVERSE CONDITIONS | DAYLIGHT | 0 | 0 |
| 1 | 1 | 0 | 0 | 1 | 0 | 0 | 1000 | NO ADVERSE CONDITIONS | DAYLIGHT | 0 | 0 |
| 2 | 1 | 0 | 0 | 1 | 0 | 0 | 815 | NO ADVERSE CONDITIONS | DAWN | 0 | 0 |
| 2 | 1 | 0 | 0 | 1 | 0 | 0 | 1700 | NO ADVERSE CONDITIONS | DAYLIGHT | 0 | 0 |
| 1 | 1 | 0 | 1 | 0 | 0 | 1 | 2346 | No Adverse conditions | dark--no Street lights | 0 | 0 |
| 2 | 1 | 0 | 0 | 1 | 0 | 0 | 1734 | NO ADVERSE CONDITIONS | dark--street lights on | 0 | 0 |
| 1 | 1 | 0 | 0 | 1 | 0 | 0 | 145 | NO ADVERSE CONDITIONS | dark--street lights on | 38.945577 | -95.204202 |
| 1 | 1 | 0 | 1 | 0 | 0 | 1 | 2346 | No Adverse conditions | dark--no Street lights | 0 | 0 |


| cident Key | Date | On Road | Dist | UOM | Dir | Accident Class | cwov | Fixed Object | Accident Location | \# of Vehs | Total Accs | Fatal <br> Accs | Injury Accs | PDO Accs | \# of Deaths | \# of Injuries | Time | Weather | Light Conditions | DOT Latitude | DOT Longitude |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 20180101182 | 1/22/2018 | 23RD | <Null> |  |  | Other Motor Vehicle | Angle - Side Impact |  | Intersection | 2 | 1 | 0 | 0 | 1 | 0 | 0 | 1135 | Rain, mist, or drizzle | Daylight | 38.942791 | -95.204919 |
| 20180121662 | 9/15/2018 | 23RD | <Null> |  |  | Other Motor Vehicle | Rear End |  | Intersection | 4 | 1 | 0 | 1 | 0 | 0 | 1 | 1917 | No adverse conditions | Dusk | 38.942791 | -95.204919 |
| 20180103846 | 2/21/2018 | 23RD | 15 | F | E | Other Motor Vehicle | Rear End |  | Intersection-related | 2 | 1 | 0 | 0 | 1 | 0 | 0 | 1831 | No adverse conditions | Dark: Street Lights On | 38.942791 | -95.204866 |
| 20180120363 | 8/28/2018 | 23RD | 20 | F | E | Other Motor Vehicle | Rear End |  | Intersection-related | 2 | 1 | 0 | 1 | 0 | 0 | 2 | 632 | No adverse conditions | Daylight | 38.94279 | -95.204848 |
| 20180104620 | 2/7/2018 | 23RD | 30 | F | E | Other Motor Vehicle | Rear End |  | Intersection-related | 2 | 1 | 0 | 0 | 1 | 0 | 0 | 1237 | No adverse conditions | Daylight | 38.94279 | -95.204813 |
| 20180117730 | 7/30/2018 | 23RD | 80 | F | w | Other Motor Vehicle | Rear End |  | Non-Intersection | 2 | 1 | 0 | 0 | 1 | 0 | 0 | 925 | No adverse conditions | Daylight | 38.942792 | -95.2052 |
| 20180100509 | 1/14/2018 | 23RD | 100 | F | w | Other Motor Vehicle | Rear End |  | Intersection-related | 2 | 1 | 0 | 0 | 1 | 0 | 0 | 1050 | Snow | Daylight | 38.942792 | -95.20527 |
| 20180101251 | 1/23/2018 | 23RD | 200 | F | w | Other Motor Vehicle | Rear End |  | Intersection-related | 2 | 1 | 0 | 0 | 1 | 0 | 0 | 1756 | No adverse conditions | Dark: Street Lights On | 38.942794 | -95.205622 |
| 20180100995 | 1/20/2018 | 23RD | 500 | F | w | Other Motor Vehicle | Rear End |  | Intersection-related | 3 | 1 | 0 | 1 | 0 | 0 | 2 | 1947 | No adverse conditions | Dark: Street Lights On | 38.942797 | -95.206677 |
| 20180117736 | 7/31/2018 | O'CONNELL | 30 | F | S | Other Motor Vehicle | Rear End |  | Intersection-related | 2 | 1 | 0 | 0 | 1 | 0 | 0 | 740 | No adverse conditions | Daylight | 38.942709 | -95.204916 |
| 20180115999 | 7/9/2018 | O'CONNELL | 30 | F | s | Other Motor Vehicle | Angle - Side Impact |  | Intersection-related | 2 | 1 | 0 | 1 | 0 | 0 | 1 | 1300 | No adverse conditions | Daylight | 38.942709 | -95.204916 |
| 20180131350 | 12/5/2018 | o'Connell | 50 | F | S | Other Motor Vehicle | Angle - Side Impact |  | Non-Intersection | 2 | 1 | 0 | 0 | 1 | 0 | 0 | 1227 | No adverse conditions | Daylight | 38.942654 | -95.204914 |
| 20180116491 | 5/24/2018 | Venturepark | 500 | F | E | Fixed Object |  | Curb | Non-Intersection | 1 | 1 | 0 | 0 | 1 | 0 | 0 | 304 | No adverse conditions | Dark: Street Lights On | 38.945562 | -95.202444 |


|  |  |  |  |  |  |  | 4 |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ | 个4 | 「 | \％ | 个4 | 「 | \％ | $\hat{\dagger}$ |  | \％ | 4 | F |
| Traffic Volume（vph） | 30 | 593 | 45 | 9 | 552 | 0 | 92 | 15 | 54 | 3 | 3 | 41 |
| Future Volume（vph） | 30 | 593 | 45 | 9 | 552 | 0 | 92 | 15 | 54 | 3 | 3 | 41 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length（ft） | 750 |  | 550 | 700 |  | 1000 | 145 |  | 0 | 270 |  | 0 |
| Storage Lanes | 1 |  | 1 | 1 |  | 1 | 1 |  | 0 | 1 |  | 1 |
| Taper Length（ft） | 220 |  |  | 220 |  |  | 25 |  |  | 65 |  |  |
| Lane Util．Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt |  |  | 0.850 |  |  |  |  | 0.883 |  |  |  | 0.850 |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd．Flow（prot） | 1770 | 3539 | 1583 | 1770 | 3539 | 1863 | 1770 | 1645 | 0 | 1770 | 1863 | 1583 |
| Flt Permitted | 0.950 |  |  | 0.950 |  |  | 0.664 |  |  | 0.709 |  |  |
| Satd．Flow（perm） | 1770 | 3539 | 1583 | 1770 | 3539 | 1863 | 1237 | 1645 | 0 | 1321 | 1863 | 1583 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd．Flow（RTOR） |  |  | 145 |  |  |  |  | 57 |  |  |  | 240 |
| Link Speed（mph） |  | 45 |  |  | 55 |  |  | 35 |  |  | 35 |  |
| Link Distance（ft） |  | 1944 |  |  | 5046 |  |  | 911 |  |  | 1100 |  |
| Travel Time（s） |  | 29.5 |  |  | 62.6 |  |  | 17.7 |  |  | 21.4 |  |
| Peak Hour Factor | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Adj．Flow（vph） | 32 | 631 | 48 | 10 | 587 | 0 | 98 | 16 | 57 | 3 | 3 | 44 |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow（vph） | 32 | 631 | 48 | 10 | 587 | 0 | 98 | 73 | 0 | 3 | 3 | 44 |
| Enter Blocked Intersectio | ono | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | Left | Left | Right | Left | Left | Right | Left | Left | Right | Left | Left | Right |
| Median Width（ft） |  | 30 |  |  | 36 |  |  | 12 |  |  | 12 |  |
| Link Offset（ft） |  | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |
| Crosswalk Width（ft） |  | 16 |  |  | 16 |  |  | 16 |  |  | 16 |  |
| Two way Left Turn Lane |  |  |  |  |  |  |  | Yes |  |  |  |  |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed（mph） | 15 |  | 9 | 15 |  | 9 | 15 |  | ， | 15 |  | 9 |
| Number of Detectors | 1 | 2 | 1 | 1 | 2 | 1 | 1 | 2 |  | 1 | 2 | 1 |
| Detector Template | Left | Thru | Right | Left | Thru | Right | Left | Thru |  | Left | Thru | Right |
| Leading Detector（ft） | 20 | 100 | 20 | 20 | 100 | 20 | 20 | 100 |  | 20 | 100 | 20 |
| Trailing Detector（ft） | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 |
| Detector 1 Position（ft） | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 |
| Detector 1 Size（ft） | 20 | 6 | 20 | 20 | 6 | 20 | 20 | 6 |  | 20 | 6 | 20 |
| Detector 1 Type | Cl＋Ex | Cl＋Ex | Cl＋Ex | Cl＋Ex | Cl＋Ex | Cl＋Ex | $\mathrm{Cl}+\mathrm{Ex}$ | Cl＋Ex |  | Cl＋Ex | Cl＋Ex | $\mathrm{Cl}+\mathrm{Ex}$ |
| Detector 1 Channel |  |  |  |  |  |  |  |  |  |  |  |  |
| Detector 1 Extend（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |
| Detector 1 Queue（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |
| Detector 1 Delay（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |
| Detector 2 Position（ft） |  | 94 |  |  | 94 |  |  | 94 |  |  | 94 |  |
| Detector 2 Size（ft） |  | 6 |  |  | 6 |  |  | 6 |  |  | 6 |  |
| Detector 2 Type |  | Cl＋Ex |  |  | Cl＋Ex |  |  | Cl＋Ex |  |  | Cl＋Ex |  |
| Detector 2 Channel |  |  |  |  |  |  |  |  |  |  |  |  |
| Detector 2 Extend（s） |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |
| Turn Type | Prot | NA | $\mathrm{pt}+\mathrm{v}$ | Prot | NA | pt＋ov | pm＋pt | NA |  | pm＋pt | NA | Prot |
| Protected Phases | 7 | 4 | 45 | 3 | 8 | 81 | 5 | 2 |  | 1 | 6 | 6 |
| Permitted Phases |  |  |  |  |  |  | 2 |  |  | 6 |  |  |


|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |


|  | 4 | $\rightarrow$ |  | $\downarrow$ |  |  | 4 | 4 | $p$ |  | $\frac{1}{1}$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.20 | 0.50 | 0.06 | 0.07 | 0.52 |  | 0.16 | 0.10 |  | 0.01 | 0.01 | 0.07 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 75 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 62.4 |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 75 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Semi Act-Uncoord |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.66 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 21.7 |  |  |  | Intersection LOS: C |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 47.5\% ICU Level of Service A |  |  |  |  |  |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |
| 90th \%ile Actuated Cycle: 75 |  |  |  |  |  |  |  |  |  |  |  |  |
| 70th \%ile Actuated Cycle: 75 |  |  |  |  |  |  |  |  |  |  |  |  |
| 50th \%ile Actuated Cycle: 60.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 30th \%ile Actuated Cycle: 58.8 |  |  |  |  |  |  |  |  |  |  |  |  |
| 10th \%ile Actuated Cycle: 42.5 |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 3: E 1600 Road/O'Connell Road \& E 23rd Street/N 1400 Road


|  | $\rangle$ |  |  |  |  |  | 4 | $\dagger$ |  |  |  | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }_{1}$ | 个个 | 「 | \％ | 个4 | 「 | \％ | $\uparrow$ |  | \％ | 4 | F |
| Traffic Volume（vph） | 12 | 769 | 94 | 69 | 723 | ， | 53 | 3 | 31 | 2 | 16 | 47 |
| Future Volume（vph） | 12 | 769 | 94 | 69 | 723 | 4 | 53 | 3 | 31 | 2 | 16 | 47 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length（ft） | 750 |  | 550 | 700 |  | 1000 | 145 |  | 0 | 270 |  | 0 |
| Storage Lanes | 1 |  | 1 | 1 |  | 1 | 1 |  | 0 | 1 |  | 1 |
| Taper Length（ft） | 220 |  |  | 220 |  |  | 25 |  |  | 65 |  |  |
| Lane Util．Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt |  |  | 0.850 |  |  | 0.850 |  | 0.862 |  |  |  | 0.850 |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd．Flow（prot） | 1770 | 3539 | 1583 | 1770 | 3539 | 1583 | 1770 | 1606 | 0 | 1770 | 1863 | 1583 |
| Flt Permitted | 0.950 |  |  | 0.950 |  |  | 0.666 |  |  | 0.734 |  |  |
| Satd．Flow（perm） | 1770 | 3539 | 1583 | 1770 | 3539 | 1583 | 1241 | 1606 | 0 | 1367 | 1863 | 1583 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd．Flow（RTOR） |  |  | 145 |  |  | 145 |  | 33 |  |  |  | 240 |
| Link Speed（mph） |  | 45 |  |  | 55 |  |  | 35 |  |  | 35 |  |
| Link Distance（ft） |  | 1944 |  |  | 5046 |  |  | 911 |  |  | 1100 |  |
| Travel Time（s） |  | 29.5 |  |  | 62.6 |  |  | 17.7 |  |  | 21.4 |  |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Adj．Flow（vph） | 13 | 809 | 99 | 73 | 761 | 4 | 56 | 3 | 33 | ， | 17 | 49 |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow（vph） | 13 | 809 | 99 | 73 | 761 | 4 | 56 | 36 | 0 | 2 | 17 | 49 |
| Enter Blocked Intersectio | on | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | Left | Left | Right | Left | Left | Right | Left | Left | Right | Left | Left | Right |
| Median Width（ft） |  | 30 |  |  | 36 |  |  | 12 |  |  | 12 |  |
| Link Offset（ft） |  | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |
| Crosswalk Width（ft） |  | 16 |  |  | 16 |  |  | 16 |  |  | 16 |  |
| Two way Left Turn Lane |  |  |  |  |  |  |  | Yes |  |  |  |  |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed（mph） | 15 |  | 9 | 15 |  | ， | 15 |  |  | 15 |  | 9 |
| Number of Detectors | 1 | 2 | 1 | 1 | 2 | 1 | 1 | 2 |  | 1 | 2 | 1 |
| Detector Template | Left | Thru | Right | Left | Thru | Right | Left | Thru |  | Left | Thru | Right |
| Leading Detector（ft） | 20 | 100 | 20 | 20 | 100 | 20 | 20 | 100 |  | 20 | 100 | 20 |
| Trailing Detector（ft） | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 |
| Detector 1 Position（ft） | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 |
| Detector 1 Size（ft） | 20 | 6 | 20 | 20 | 6 | 20 | 20 | 6 |  | 20 | 6 | 20 |
| Detector 1 Type | Cl＋Ex | Cl＋Ex | Cl＋Ex | Cl＋Ex | Cl＋Ex | $\mathrm{Cl}+\mathrm{Ex}$ | $\mathrm{Cl}+\mathrm{Ex}$ | Cl＋Ex |  | Cl＋Ex | Cl＋Ex | Cl＋Ex |
| Detector 1 Channel |  |  |  |  |  |  |  |  |  |  |  |  |
| Detector 1 Extend（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |
| Detector 1 Queue（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |
| Detector 1 Delay（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |
| Detector 2 Position（ft） |  | 94 |  |  | 94 |  |  | 94 |  |  | 94 |  |
| Detector 2 Size（ft） |  | 6 |  |  | 6 |  |  | 6 |  |  | 6 |  |
| Detector 2 Type |  | Cl＋Ex |  |  | Cl＋Ex |  |  | Cl＋Ex |  |  | Cl＋Ex |  |
| Detector 2 Channel |  |  |  |  |  |  |  |  |  |  |  |  |
| Detector 2 Extend（s） |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |
| Turn Type | Prot | NA | pt＋ov | Prot | NA | pt＋ov | pm＋pt | NA |  | pm＋pt | NA | Prot |
| Protected Phases | 7 | 4 | 45 | 3 | 8 | 81 | 5 | 2 |  | 1 | 6 | 6 |
| Permitted Phases |  |  |  |  |  |  | 2 |  |  | 6 |  |  |


|  | 4 |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Detector Phase | 7 | 4 | 45 | 3 | 8 | 81 | 5 | 2 |  | 1 | 6 | 6 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 | 5.0 |
| Minimum Split (s) | 11.5 | 25.0 |  | 11.5 | 25.0 |  | 11.5 | 25.0 |  | 11.5 | 25.0 | 25.0 |
| Total Split (s) | 11.5 | 26.0 |  | 12.2 | 26.7 |  | 11.5 | 25.3 |  | 11.5 | 25.3 | 25.3 |
| Total Split (\%) | 15.3\% | 34.7\% |  | 16.3\% | 35.6\% |  | 15.3\% | 33.7\% |  | 15.3\% | 33.7\% | 33.7\% |
| Maximum Green (s) | 5.0 | 19.5 |  | 5.7 | 20.2 |  | 5.0 | 18.8 |  | 5.0 | 18.8 | 18.8 |
| Yellow Time (s) | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 |
| All-Red Time (s) | 2.5 | 2.5 |  | 2.5 | 2.5 |  | 2.5 | 2.5 |  | 2.5 | 2.5 | 2.5 |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 6.5 | 6.5 |  | 6.5 | 6.5 |  | 6.5 | 6.5 |  | 6.5 | 6.5 | 6.5 |
| Lead/Lag | Lead | Lag |  | Lead | Lag |  | Lead | Lag |  | Lead | Lag | Lag |
| Lead-Lag Optimize? | Yes | Yes |  | Yes | Yes |  | Yes | Yes |  | Yes | Yes | Yes |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None |  | None | None |  | None | Max |  | None | Max | Max |
| Walk Time (s) |  | 7.0 |  |  | 7.0 |  |  | 7.0 |  |  | 7.0 | 7.0 |
| Flash Dont Walk (s) |  | 11.0 |  |  | 11.0 |  |  | 11.0 |  |  | 11.0 | 11.0 |
| Pedestrian Calls (\#/hr) |  | 0 |  |  | 0 |  |  | 0 |  |  | 0 | 0 |
| Act Effct Green (s) | 5.2 | 18.6 | 30.6 | 5.9 | 25.5 | 37.5 | 26.8 | 25.9 |  | 23.2 | 19.6 | 19.6 |
| Actuated g/C Ratio | 0.08 | 0.27 | 0.44 | 0.09 | 0.37 | 0.54 | 0.39 | 0.37 |  | 0.34 | 0.28 | 0.28 |
| v/c Ratio | 0.10 | 0.85 | 0.13 | 0.49 | 0.58 | 0.00 | 0.11 | 0.06 |  | 0.00 | 0.03 | 0.08 |
| Control Delay | 34.8 | 35.8 | 1.5 | 45.8 | 21.0 | 0.0 | 14.6 | 8.3 |  | 13.5 | 21.6 | 0.3 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |
| Total Delay | 34.8 | 35.8 | 1.5 | 45.8 | 21.0 | 0.0 | 14.6 | 8.3 |  | 13.5 | 21.6 | 0.3 |
| LOS | C | D | A | D | C | A | B | A |  | B | C | A |
| Approach Delay |  | 32.1 |  |  | 23.1 |  |  | 12.1 |  |  | 6.0 |  |
| Approach LOS |  | C |  |  | C |  |  | B |  |  | A |  |
| 90th \%ile Green (s) | 5.0 | 19.5 |  | 5.7 | 20.2 |  | 5.0 | 18.8 |  | 5.0 | 18.8 | 18.8 |
| 90th \%ile Term Code | Max | Max |  | Max | Max |  | Max | MaxR |  | Max | MaxR | MaxR |
| 70th \%ile Green (s) | 0.0 | 19.5 |  | 5.7 | 31.7 |  | 5.0 | 30.3 |  | 0.0 | 18.8 | 18.8 |
| 70th \%ile Term Code | Skip | Max |  | Max | Hold |  | Max | Hold |  | Skip | MaxR | MaxR |
| 50th \%ile Green (s) | 0.0 | 19.5 |  | 5.7 | 31.7 |  | 5.0 | 30.3 |  | 0.0 | 18.8 | 18.8 |
| 50th \%ile Term Code | Skip | Max |  | Max | Hold |  | Max | Hold |  | Skip | MaxR | MaxR |
| 30th \%ile Green (s) | 0.0 | 19.5 |  | 5.7 | 31.7 |  | 5.0 | 30.3 |  | 0.0 | 18.8 | 18.8 |
| 30th \%ile Term Code | Skip | Max |  | Max | Hold |  | Max | Hold |  | Skip | MaxR | MaxR |
| 10th \%ile Green (s) | 0.0 | 14.0 |  | 0.0 | 14.0 |  | 0.0 | 18.8 |  | 0.0 | 18.8 | 18.8 |
| 10th \%ile Term Code | Skip | Gap |  | Skip | Hold |  | Skip | MaxR |  | Skip | MaxR | MaxR |
| Stops (vph) | 14 | 660 | 5 | 64 | 532 | 0 | 33 | 10 |  | 3 | 14 | 0 |
| Fuel Used(gal) | 0 | 24 | 1 | 4 | 36 | 0 | 1 | 0 |  | 0 | 0 | 0 |
| CO Emissions (g/hr) | 29 | 1644 | 89 | 282 | 2523 | 9 | 53 | 25 |  | 3 | 21 | 26 |
| NOx Emissions (g/hr) | 6 | 320 | 17 | 55 | 491 | 2 | 10 | 5 |  | 1 | 4 | 5 |
| VOC Emissions (g/hr) | 7 | 381 | 21 | 65 | 585 | 2 | 12 | 6 |  | , |  | 6 |
| Dilemma Vehicles (\#) | 0 | 51 | 0 | 0 | 46 | 0 | 0 | 2 |  | 0 | 1 | 0 |
| Queue Length 50th (ft) | 6 | 190 | 0 | 34 | 132 | 0 | 16 | 1 |  | 1 | 6 | 0 |
| Queue Length 95th (ft) | 22 | \#291 | 13 | \#85 | \#243 | 0 | 37 | 22 |  | 4 | 21 | 0 |
| Internal Link Dist (ft) |  | 1864 |  |  | 4966 |  |  | 831 |  |  | 1020 |  |
| Turn Bay Length (ft) | 750 |  | 550 | 700 |  | 1000 | 145 |  |  | 270 |  |  |
| Base Capacity (vph) | 133 | 1037 | 774 | 151 | 1400 | 921 | 521 | 622 |  | 489 | 526 | 619 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 |



Splits and Phases: 3: E 1600 Road/O'Connell Road \& E 23rd Street/N 1400 Road


|  |  |  | 7 |  |  |  | 4 |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ | 个4 | ${ }^{*}$ | \％ | 个4 | 「 | \％ | $\hat{\beta}$ |  | \％ | 4 | F |
| Traffic Volume（vph） | 108 | 593 | 45 | 9 | 552 | 66 | 92 | 34 | 54 | 67 | 8 | 108 |
| Future Volume（vph） | 108 | 593 | 45 | 9 | 552 | 66 | 92 | 34 | 54 | 67 | 8 | 108 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length（ft） | 750 |  | 550 | 700 |  | 1000 | 145 |  | 0 | 270 |  | 0 |
| Storage Lanes | 1 |  | 1 | 1 |  | 1 | 1 |  | 0 | 1 |  | 1 |
| Taper Length（ft） | 220 |  |  | 220 |  |  | 25 |  |  | 65 |  |  |
| Lane Util．Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt |  |  | 0.850 |  |  | 0.850 |  | 0.908 |  |  |  | 0.850 |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd．Flow（prot） | 1770 | 3539 | 1583 | 1770 | 3539 | 1583 | 1770 | 1691 | 0 | 1770 | 1863 | 1583 |
| Flt Permitted | 0.950 |  |  | 0.950 |  |  | 0.752 |  |  | 0.697 |  |  |
| Satd．Flow（perm） | 1770 | 3539 | 1583 | 1770 | 3539 | 1583 | 1401 | 1691 | 0 | 1298 | 1863 | 1583 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd．Flow（RTOR） |  |  | 145 |  |  | 145 |  | 57 |  |  |  | 240 |
| Link Speed（mph） |  | 45 |  |  | 55 |  |  | 35 |  |  | 35 |  |
| Link Distance（ft） |  | 1944 |  |  | 5046 |  |  | 911 |  |  | 1100 |  |
| Travel Time（s） |  | 29.5 |  |  | 62.6 |  |  | 17.7 |  |  | 21.4 |  |
| Peak Hour Factor | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Adj．Flow（vph） | 115 | 631 | 48 | 10 | 587 | 70 | 98 | 36 | 57 | 71 | 9 | 115 |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow（vph） | 115 | 631 | 48 | 10 | 587 | 70 | 98 | 93 | 0 | 71 | 9 | 115 |
| Enter Blocked Intersectio | on No | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | Left | Left | Right | Left | Left | Right | Left | Left | Right | Left | Left | Right |
| Median Width（ft） |  | 30 |  |  | 36 |  |  | 12 |  |  | 12 |  |
| Link Offset（ft） |  | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |
| Crosswalk Width（ft） |  | 16 |  |  | 16 |  |  | 16 |  |  | 16 |  |
| Two way Left Turn Lane |  |  |  |  |  |  |  | Yes |  |  |  |  |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed（mph） | 15 |  | 9 | 15 |  | 9 | 15 |  | ， | 15 |  | 9 |
| Number of Detectors | 1 | 2 | 1 | 1 | 2 | 1 | 1 | 2 |  | 1 | 2 | 1 |
| Detector Template | Left | Thru | Right | Left | Thru | Right | Left | Thru |  | Left | Thru | Right |
| Leading Detector（ft） | 20 | 100 | 20 | 20 | 100 | 20 | 20 | 100 |  | 20 | 100 | 20 |
| Trailing Detector（ft） | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 |
| Detector 1 Position（ft） | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 |
| Detector 1 Size（ft） | 20 | 6 | 20 | 20 | ， | 20 | 20 | 6 |  | 20 | 6 | 20 |
| Detector 1 Type | Cl＋Ex | Cl＋Ex | Cl＋Ex | Cl＋Ex | Cl＋Ex | Cl＋Ex | $\mathrm{Cl}+\mathrm{Ex}$ | Cl＋Ex |  | Cl＋Ex | Cl＋Ex | $\mathrm{Cl}+\mathrm{Ex}$ |
| Detector 1 Channel |  |  |  |  |  |  |  |  |  |  |  |  |
| Detector 1 Extend（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |
| Detector 1 Queue（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |
| Detector 1 Delay（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |
| Detector 2 Position（ft） |  | 94 |  |  | 94 |  |  | 94 |  |  | 94 |  |
| Detector 2 Size（ft） |  | 6 |  |  | 6 |  |  | 6 |  |  | 6 |  |
| Detector 2 Type |  | Cl＋Ex |  |  | Cl＋Ex |  |  | Cl＋Ex |  |  | Cl＋Ex |  |
| Detector 2 Channel |  |  |  |  |  |  |  |  |  |  |  |  |
| Detector 2 Extend（s） |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |
| Turn Type | Prot | NA | pt＋ov | Prot | NA | $\mathrm{pt+ov}$ | pm＋pt | NA |  | pm＋pt | NA | Prot |
| Protected Phases | 7 | 4 | 45 | 3 | 8 | 81 | 5 | 2 |  | 1 | 6 | 6 |
| Permitted Phases |  |  |  |  |  |  | 2 |  |  | 6 |  |  |


|  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Detector Phase | 7 | 4 | 45 | 3 | 8 | 81 | 5 | 2 |  | 1 | 6 | 6 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 | 5.0 |
| Minimum Split (s) | 11.5 | 25.0 |  | 11.5 | 25.0 |  | 11.5 | 25.0 |  | 11.5 | 25.0 | 25.0 |
| Total Split (s) | 13.0 | 26.5 |  | 11.5 | 25.0 |  | 11.5 | 25.5 |  | 11.5 | 25.5 | 25.5 |
| Total Split (\%) | 17.3\% | 35.3\% |  | 15.3\% | 33.3\% |  | 15.3\% | 34.0\% |  | 15.3\% | 34.0\% | 34.0\% |
| Maximum Green (s) | 6.5 | 20.0 |  | 5.0 | 18.5 |  | 5.0 | 19.0 |  | 5.0 | 19.0 | 19.0 |
| Yellow Time (s) | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 |
| All-Red Time (s) | 2.5 | 2.5 |  | 2.5 | 2.5 |  | 2.5 | 2.5 |  | 2.5 | 2.5 | 2.5 |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 6.5 | 6.5 |  | 6.5 | 6.5 |  | 6.5 | 6.5 |  | 6.5 | 6.5 | 6.5 |
| Lead/Lag | Lead | Lag |  | Lead | Lag |  | Lead | Lag |  | Lead | Lag | Lag |
| Lead-Lag Optimize? | Yes | Yes |  | Yes | Yes |  | Yes | Yes |  | Yes | Yes | Yes |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None |  | None | None |  | None | Max |  | None | Max | Max |
| Walk Time (s) |  | 7.0 |  |  | 7.0 |  |  | 7.0 |  |  | 7.0 | 7.0 |
| Flash Dont Walk (s) |  | 11.0 |  |  | 11.0 |  |  | 11.0 |  |  | 11.0 | 11.0 |
| Pedestrian Calls (\#/hr) |  | 0 |  |  | 0 |  |  | 0 |  |  | 0 | 0 |
| Act Effct Green (s) | 6.8 | 23.8 | 35.9 | 5.2 | 16.3 | 28.4 | 23.6 | 19.9 |  | 23.6 | 19.9 | 19.9 |
| Actuated g/C Ratio | 0.10 | 0.35 | 0.53 | 0.08 | 0.24 | 0.42 | 0.35 | 0.29 |  | 0.35 | 0.29 | 0.29 |
| v/c Ratio | 0.65 | 0.51 | 0.05 | 0.07 | 0.69 | 0.09 | 0.19 | 0.17 |  | 0.15 | 0.02 | 0.18 |
| Control Delay | 53.2 | 19.9 | 0.1 | 34.2 | 29.6 | 0.2 | 15.3 | 11.8 |  | 14.8 | 21.2 | 0.6 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |
| Total Delay | 53.2 | 19.9 | 0.1 | 34.2 | 29.6 | 0.2 | 15.3 | 11.8 |  | 14.8 | 21.2 | 0.6 |
| LOS | D | B | A | C | C | A | B | B |  | B | C | A |
| Approach Delay |  | 23.5 |  |  | 26.6 |  |  | 13.6 |  |  | 6.7 |  |
| Approach LOS |  | C |  |  | C |  |  | B |  |  | A |  |
| 90th \%ile Green (s) | 6.5 | 20.0 |  | 5.0 | 18.5 |  | 5.0 | 19.0 |  | 5.0 | 19.0 | 19.0 |
| 90th \%ile Term Code | Max | Max |  | Max | Max |  | Max | MaxR |  | Max | MaxR | MaxR |
| 70th \%ile Green (s) | 6.5 | 31.5 |  | 0.0 | 18.5 |  | 5.0 | 19.0 |  | 5.0 | 19.0 | 19.0 |
| 70th \%ile Term Code | Max | Hold |  | Skip | Max |  | Max | MaxR |  | Max | MaxR | MaxR |
| 50th \%ile Green (s) | 6.5 | 31.2 |  | 0.0 | 18.2 |  | 5.0 | 19.0 |  | 5.0 | 19.0 | 19.0 |
| 50th \%ile Term Code | Max | Hold |  | Skip | Gap |  | Max | MaxR |  | Max | MaxR | MaxR |
| 30th \%ile Green (s) | 6.5 | 28.1 |  | 0.0 | 15.1 |  | 5.0 | 19.0 |  | 5.0 | 19.0 | 19.0 |
| 30th \%ile Term Code | Max | Hold |  | Skip | Gap |  | Max | MaxR |  | Max | MaxR | MaxR |
| 10th \%ile Green (s) | 0.0 | 11.0 |  | 0.0 | 11.0 |  | 0.0 | 19.0 |  | 0.0 | 19.0 | 19.0 |
| 10th \%ile Term Code | Skip | Hold |  | Skip | Gap |  | Skip | MaxR |  | Skip | MaxR | MaxR |
| Stops (vph) | 88 | 432 | 0 | 12 | 472 | 0 | 59 | 33 |  | 43 | 8 | 0 |
| Fuel Used(gal) | 4 | 15 | 1 | 1 | 30 | 2 | 1 | 1 |  | 1 | 0 | 1 |
| CO Emissions (g/hr) | 253 | 1066 | 40 | 40 | 2079 | 148 | 93 | 72 |  | 74 | 11 | 61 |
| NOx Emissions (g/hr) | 49 | 207 | 8 | 8 | 404 | 29 | 18 | 14 |  | 14 |  | 12 |
| VOC Emissions (g/hr) | 59 | 247 | 9 | 9 | 482 | 34 | 22 | 17 |  | 17 |  | 14 |
| Dilemma Vehicles (\#) | 0 | 37 | 0 | 0 | 37 | 0 | 0 | 6 |  | 0 | 0 | 0 |
| Queue Length 50th (ft) | 53 | 105 | 0 | 5 | 130 | 0 | 28 | 13 |  | 20 | 3 | 0 |
| Queue Length 95th (ft) | \#135 | 192 | 0 | 19 | 183 | 1 | 57 | 47 |  | 44 | 14 | 0 |
| Internal Link Dist (ft) |  | 1864 |  |  | 4966 |  |  | 831 |  |  | 1020 |  |
| Turn Bay Length (ft) | 750 |  | 550 | 700 |  | 1000 | 145 |  |  | 270 |  |  |
| Base Capacity (vph) | 177 | 1388 | 904 | 136 | 1011 | 710 | 515 | 536 |  | 487 | 546 | 634 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 |



Splits and Phases: 3: E 1600 Road/O'Connell Road \& E 23rd Street/N 1400 Road


|  |  |  |  |  |  |  | 4 |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ | 个4 | 「 | \％ | 个4 | 「 | \％ | $\hat{F}$ |  | \％ | 4 | F |
| Traffic Volume（vph） | 67 | 769 | 94 | 69 | 723 | 54 | 53 | 8 | 31 | 64 | 18 | 111 |
| Future Volume（vph） | 67 | 769 | 94 | 69 | 723 | 54 | 53 | 8 | 31 | 64 | 18 | 111 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length（ft） | 750 |  | 550 | 700 |  | 1000 | 145 |  | 0 | 270 |  | 0 |
| Storage Lanes | 1 |  | 1 | 1 |  | 1 | 1 |  | 0 | 1 |  | 1 |
| Taper Length（ft） | 220 |  |  | 220 |  |  | 25 |  |  | 65 |  |  |
| Lane Util．Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt |  |  | 0.850 |  |  | 0.850 |  | 0.879 |  |  |  | 0.850 |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd．Flow（prot） | 1770 | 3539 | 1583 | 1770 | 3539 | 1583 | 1770 | 1637 | 0 | 1770 | 1863 | 1583 |
| Flt Permitted | 0.950 |  |  | 0.950 |  |  | 0.745 |  |  | 0.730 |  |  |
| Satd．Flow（perm） | 1770 | 3539 | 1583 | 1770 | 3539 | 1583 | 1388 | 1637 | 0 | 1360 | 1863 | 1583 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd．Flow（RTOR） |  |  | 145 |  |  | 145 |  | 33 |  |  |  | 240 |
| Link Speed（mph） |  | 45 |  |  | 55 |  |  | 35 |  |  | 35 |  |
| Link Distance（ft） |  | 1944 |  |  | 5046 |  |  | 911 |  |  | 1100 |  |
| Travel Time（s） |  | 29.5 |  |  | 62.6 |  |  | 17.7 |  |  | 21.4 |  |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Adj．Flow（vph） | 71 | 809 | 99 | 73 | 761 | 57 | 56 | 8 | 33 | 67 | 19 | 117 |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow（vph） | 71 | 809 | 99 | 73 | 761 | 57 | 56 | 41 | 0 | 67 | 19 | 117 |
| Enter Blocked Intersectio | on | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | Left | Left | Right | Left | Left | Right | Left | Left | Right | Left | Left | Right |
| Median Width（ft） |  | 30 |  |  | 36 |  |  | 12 |  |  | 12 |  |
| Link Offset（ft） |  | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |
| Crosswalk Width（ft） |  | 16 |  |  | 16 |  |  | 16 |  |  | 16 |  |
| Two way Left Turn Lane |  |  |  |  |  |  |  | Yes |  |  |  |  |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed（mph） | 15 |  | 9 | 15 |  | 9 | 15 |  | 9 | 15 |  | 9 |
| Number of Detectors | 1 | 2 | 1 | 1 | 2 | 1 | 1 | 2 |  | 1 | 2 | 1 |
| Detector Template | Left | Thru | Right | Left | Thru | Right | Left | Thru |  | Left | Thru | Right |
| Leading Detector（ft） | 20 | 100 | 20 | 20 | 100 | 20 | 20 | 100 |  | 20 | 100 | 20 |
| Trailing Detector（ft） | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 |
| Detector 1 Position（ft） | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 |
| Detector 1 Size（ft） | 20 | 6 | 20 | 20 | 6 | 20 | 20 | 6 |  | 20 | 6 | 20 |
| Detector 1 Type | Cl＋Ex | Cl＋Ex | Cl＋Ex | Cl＋Ex | Cl＋Ex | Cl＋Ex | $\mathrm{Cl}+\mathrm{Ex}$ | Cl＋Ex |  | Cl＋Ex | Cl＋Ex | $\mathrm{Cl}+\mathrm{Ex}$ |
| Detector 1 Channel |  |  |  |  |  |  |  |  |  |  |  |  |
| Detector 1 Extend（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |
| Detector 1 Queue（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |
| Detector 1 Delay（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |
| Detector 2 Position（ft） |  | 94 |  |  | 94 |  |  | 94 |  |  | 94 |  |
| Detector 2 Size（ft） |  | 6 |  |  | 6 |  |  | 6 |  |  | 6 |  |
| Detector 2 Type |  | Cl＋Ex |  |  | Cl＋Ex |  |  | CI＋Ex |  |  | Cl＋Ex |  |
| Detector 2 Channel |  |  |  |  |  |  |  |  |  |  |  |  |
| Detector 2 Extend（s） |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |
| Turn Type | Prot | NA | $\mathrm{pt}+\mathrm{v}$ | Prot | NA | $\mathrm{pt+ov}$ | pm＋pt | NA |  | pm＋pt | NA | Prot |
| Protected Phases | 7 | 4 | 45 | 3 | 8 | 81 | 5 | 2 |  | 1 | 6 | 6 |
| Permitted Phases |  |  |  |  |  |  | 2 |  |  | 6 |  |  |


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Splits and Phases: 3: E 1600 Road/O'Connell Road \& E 23rd Street/N 1400 Road


|  |  |  | 7 | $\downarrow$ |  |  | 4 |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ | 个4 | ${ }^{*}$ | ${ }^{7}$ | 个4 | 「 | \％ | $\stackrel{\rightharpoonup}{1}$ |  | \％ | 4 | F |
| Traffic Volume（vph） | 134 | 735 | 56 | 11 | 684 | 81 | 114 | 42 | 67 | 84 | 11 | 136 |
| Future Volume（vph） | 134 | 735 | 56 | 11 | 684 | 81 | 114 | 42 | 67 | 84 | 11 | 136 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length（ft） | 750 |  | 550 | 700 |  | 1000 | 145 |  | 0 | 270 |  | 0 |
| Storage Lanes | 1 |  | 1 | 1 |  | 1 | 1 |  | 0 | 1 |  | 1 |
| Taper Length（ft） | 220 |  |  | 220 |  |  | 25 |  |  | 65 |  |  |
| Lane Util．Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt |  |  | 0.850 |  |  | 0.850 |  | 0.908 |  |  |  | 0.850 |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd．Flow（prot） | 1770 | 3539 | 1583 | 1770 | 3539 | 1583 | 1770 | 1691 | 0 | 1770 | 1863 | 1583 |
| Flt Permitted | 0.950 |  |  | 0.950 |  |  | 0.750 |  |  | 0.682 |  |  |
| Satd．Flow（perm） | 1770 | 3539 | 1583 | 1770 | 3539 | 1583 | 1397 | 1691 | 0 | 1270 | 1863 | 1583 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd．Flow（RTOR） |  |  | 145 |  |  | 145 |  | 71 |  |  |  | 240 |
| Link Speed（mph） |  | 45 |  |  | 55 |  |  | 35 |  |  | 35 |  |
| Link Distance（ft） |  | 1944 |  |  | 5046 |  |  | 911 |  |  | 1100 |  |
| Travel Time（s） |  | 29.5 |  |  | 62.6 |  |  | 17.7 |  |  | 21.4 |  |
| Peak Hour Factor | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Adj．Flow（vph） | 143 | 782 | 60 | 12 | 728 | 86 | 121 | 45 | 71 | 89 | 12 | 145 |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow（vph） | 143 | 782 | 60 | 12 | 728 | 86 | 121 | 116 | 0 | 89 | 12 | 145 |
| Enter Blocked Intersectio | on No | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | Left | Left | Right | Left | Left | Right | Left | Left | Right | Left | Left | Right |
| Median Width（ft） |  | 30 |  |  | 36 |  |  | 12 |  |  | 12 |  |
| Link Offset（ft） |  | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |
| Crosswalk Width（ft） |  | 16 |  |  | 16 |  |  | 16 |  |  | 16 |  |
| Two way Left Turn Lane |  |  |  |  |  |  |  | Yes |  |  |  |  |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed（mph） | 15 |  | 9 | 15 |  | 9 | 15 |  | 9 | 15 |  | 9 |
| Number of Detectors | 1 | 2 | 1 | 1 | 2 | 1 | 1 | 2 |  | 1 | 2 | 1 |
| Detector Template | Left | Thru | Right | Left | Thru | Right | Left | Thru |  | Left | Thru | Right |
| Leading Detector（ft） | 20 | 100 | 20 | 20 | 100 | 20 | 20 | 100 |  | 20 | 100 | 20 |
| Trailing Detector（ft） | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 |
| Detector 1 Position（ft） | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 |
| Detector 1 Size（ft） | 20 | 6 | 20 | 20 | 6 | 20 | 20 | 6 |  | 20 | 6 | 20 |
| Detector 1 Type | Cl＋Ex | Cl＋Ex | Cl＋Ex | Cl＋Ex | Cl＋Ex | Cl＋Ex | $\mathrm{Cl}+\mathrm{Ex}$ | Cl＋Ex |  | Cl＋Ex | Cl＋Ex | $\mathrm{Cl}+\mathrm{Ex}$ |
| Detector 1 Channel |  |  |  |  |  |  |  |  |  |  |  |  |
| Detector 1 Extend（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |
| Detector 1 Queue（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |
| Detector 1 Delay（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |
| Detector 2 Position（ft） |  | 94 |  |  | 94 |  |  | 94 |  |  | 94 |  |
| Detector 2 Size（ft） |  | 6 |  |  | 6 |  |  | 6 |  |  | 6 |  |
| Detector 2 Type |  | Cl＋Ex |  |  | Cl＋Ex |  |  | Cl＋Ex |  |  | Cl＋Ex |  |
| Detector 2 Channel |  |  |  |  |  |  |  |  |  |  |  |  |
| Detector 2 Extend（s） |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |
| Turn Type | Prot | NA | pt＋ov | Prot | NA | $\mathrm{pt+ov}$ | pm＋pt | NA |  | pm＋pt | NA | Prot |
| Protected Phases | 7 | 4 | 45 | 3 | 8 | 81 | 5 | 2 |  | 1 | 6 | 6 |
| Permitted Phases |  |  |  |  |  |  | 2 |  |  | 6 |  |  |


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Splits and Phases: 3: E 1600 Road/O'Connell Road \& E 23rd Street/N 1400 Road


|  | $\rangle$ |  |  |  |  |  | 4 |  |  |  |  | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ | ¢ $\uparrow$ | 「 | \％ | 个4 | 「 | \％ | $\hat{\dagger}$ |  | \％ | 4 | F |
| Traffic Volume（vph） | 84 | 954 | 117 | 86 | 897 | 67 | 66 | 11 | 38 | 79 | 23 | 137 |
| Future Volume（vph） | 84 | 954 | 117 | 86 | 897 | 67 | 66 | 11 | 38 | 79 | 23 | 137 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length（ft） | 750 |  | 550 | 700 |  | 1000 | 145 |  | 0 | 270 |  | 0 |
| Storage Lanes | 1 |  | 1 | 1 |  | 1 | 1 |  | 0 | 1 |  | 1 |
| Taper Length（ft） | 220 |  |  | 220 |  |  | 25 |  |  | 65 |  |  |
| Lane Util．Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt |  |  | 0.850 |  |  | 0.850 |  | 0.884 |  |  |  | 0.850 |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd．Flow（prot） | 1770 | 3539 | 1583 | 1770 | 3539 | 1583 | 1770 | 1647 | 0 | 1770 | 1863 | 1583 |
| Flt Permitted | 0.950 |  |  | 0.950 |  |  | 0.741 |  |  | 0.722 |  |  |
| Satd．Flow（perm） | 1770 | 3539 | 1583 | 1770 | 3539 | 1583 | 1380 | 1647 | 0 | 1345 | 1863 | 1583 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd．Flow（RTOR） |  |  | 136 |  |  | 136 |  | 41 |  |  |  | 225 |
| Link Speed（mph） |  | 45 |  |  | 55 |  |  | 35 |  |  | 35 |  |
| Link Distance（ft） |  | 1944 |  |  | 5046 |  |  | 911 |  |  | 1100 |  |
| Travel Time（s） |  | 29.5 |  |  | 62.6 |  |  | 17.7 |  |  | 21.4 |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj．Flow（vph） | 91 | 1037 | 127 | 93 | 975 | 73 | 72 | 12 | 41 | 86 | 25 | 149 |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow（vph） | 91 | 1037 | 127 | 93 | 975 | 73 | 72 | 53 | 0 | 86 | 25 | 149 |
| Enter Blocked Intersectio | n No | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | Left | Left | Right | Left | Left | Right | Left | Left | Right | Left | Left | Right |
| Median Width（ft） |  | 30 |  |  | 36 |  |  | 12 |  |  | 12 |  |
| Link Offset（ft） |  | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |
| Crosswalk Width（ft） |  | 16 |  |  | 16 |  |  | 16 |  |  | 16 |  |
| Two way Left Turn Lane |  |  |  |  |  |  |  | Yes |  |  |  |  |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed（mph） | 15 |  | 9 | 15 |  | 9 | 15 |  |  | 15 |  | 9 |
| Number of Detectors | 1 | 2 | 1 | 1 | 2 | 1 | 1 | 2 |  | 1 | 2 | 1 |
| Detector Template | Left | Thru | Right | Left | Thru | Right | Left | Thru |  | Left | Thru | Right |
| Leading Detector（ft） | 20 | 100 | 20 | 20 | 100 | 20 | 20 | 100 |  | 20 | 100 | 20 |
| Trailing Detector（ft） | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 |
| Detector 1 Position（ft） | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 |
| Detector 1 Size（ft） | 20 | 6 | 20 | 20 | 6 | 20 | 20 | 6 |  | 20 | 6 | 20 |
| Detector 1 Type | Cl＋Ex | Cl＋Ex | Cl＋Ex | Cl＋Ex | Cl＋Ex | Cl＋Ex | $\mathrm{Cl}+\mathrm{Ex}$ | Cl＋Ex |  | Cl＋Ex | Cl＋Ex | Cl＋Ex |
| Detector 1 Channel |  |  |  |  |  |  |  |  |  |  |  |  |
| Detector 1 Extend（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |
| Detector 1 Queue（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |
| Detector 1 Delay（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |
| Detector 2 Position（ft） |  | 94 |  |  | 94 |  |  | 94 |  |  | 94 |  |
| Detector 2 Size（ft） |  | 6 |  |  | 6 |  |  | 6 |  |  | 6 |  |
| Detector 2 Type |  | Cl＋Ex |  |  | Cl＋Ex |  |  | Cl＋Ex |  |  | Cl＋Ex |  |
| Detector 2 Channel |  |  |  |  |  |  |  |  |  |  |  |  |
| Detector 2 Extend（s） |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |
| Turn Type | Prot | NA | pt＋ov | Prot | NA | pt＋ov | pm＋pt | NA |  | pm＋pt | NA | Prot |
| Protected Phases | 7 | 4 | 45 | ， | 8 | 81 | 5 | 2 |  | 1 | 6 | 6 |
| Permitted Phases |  |  |  |  |  |  | 2 |  |  | 6 |  |  |


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|  |  |  |  |  |  |  |  | $\uparrow$ | $p$ |  |  | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.68 | 0.87 | 0.16 | 0.69 | 0.81 | 0.09 | 0.16 | 0.11 |  | 0.19 | 0.05 | 0.26 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 80 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 74.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 80 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Semi Act-Uncoord |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.91 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 32.6 |  |  |  |  | Intersection LOS: C |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 58.4\% ICU Level of Service B |  |  |  |  |  |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |
| 90th \%ile Actuated Cycle: 80 |  |  |  |  |  |  |  |  |  |  |  |  |
| 70th \%ile Actuated Cycle: 80 |  |  |  |  |  |  |  |  |  |  |  |  |
| 50th \%ile Actuated Cycle: 80 |  |  |  |  |  |  |  |  |  |  |  |  |
| 30th \%ile Actuated Cycle: 80 |  |  |  |  |  |  |  |  |  |  |  |  |
| 10th \%ile Actuated Cycle: 52.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 3: E 1600 Road/O'Connell Road \& E 23rd Street/N 1400 Road




[^0]:    *Pedestrians and Bicycles on Crosswalk. L: Left, R: Right, T: Thru, U: U-Turn

